

DOCTORAL (Ph.D.) DISSERTATION

Optimization of manufacture and examination of micropellets based on pharmaceutical technological and biopharmaceutical parameters

Dr. Szilárd Pál



University of Pécs, Faculty of Medicine

Institute of Pharmaceutical Technology and Biopharmacy

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Dr. Szilárd Pál



Head of the Doctoral School:

Dr. Erika Pintér

Head of Program:

Dr. Loránd Barthó

Supervisor:

Dr. Attila Dévay

Founder and first director of
the Institute of Pharmaceutical Technology and Biopharmacy
University of Pécs, Faculty of Medicine

Pécs

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List of Abbreviations

| | |
|-------------|---|
| ATCC | American Type Culture Collection |
| API | Active Pharmaceutical Ingredient |
| BCS | Biopharmaceutical Classification System |
| CPL | CarboPoL®/carbomer |
| DOE | Design Of Experiment |
| EC | EthylCellulose |
| ED | Experimental Design |
| EDTA | EthyleneDiamineTetraacetic Acid |
| FBMR | Focused Beam Reflectance Measurement |
| GI | GastroIntestinal |
| GIC | GastroIntestinal Candidiasis |
| HEC | HydroxyEthylCellulose |
| HIV | Human Immunodeficiency Virus |
| MDD | Microbiologically Detected Dissolution |
| MDT | Mean Dissolution Time |
| MTT | 3-(4,5-diMethylThiazol-2-yl)-2,5-diphenylTetrazolium bromide |
| NIR | Near Infrared |
| NIRS | Near Infrared Spectroscopy |
| NS | Not Significant |

| | |
|---|---|
| RH | Relative Humidity |
| RPM | Rotation Per Minute |
| RRSB | Rosin-Rammler-Bennett-Sperling |
| RSV | Relative Swept Volume |
| SEM | Scanning Electron Microscope |
| S.D. | Standard Deviation |
| τ, τ_D | Mean Dissolution Time (MDT) |
| τ_M | MDT based on microbiological examinations |
| τ_S | MDT based on spectrophotometric examinations |
| TLC | Thin Layer Chromatography |
| UV | Ultra Violet |
| VIS | VISible |

1. Introduction

Optimization of the drug release of peroral dosage forms and adjusting it to the absorption window of the active ingredient is the fundamental point in the development of a new pharmaceutical product [1,2]. However, there may be different aspects in cases when local effect is required. In this type of therapy the concept of the dissolution of active ingredients should be reevaluated [3]. The enhancement of the bioavailability according to the Biopharmaceutical Classification System (BCS) [4] cannot be applied invariably [6], since importance of the absorption and the permeability is minor. Conversely, there are other essential parameters which should be taken into account during the development of these preparations, including the adhesivity to the mucous membrane, large contact surface of the drug particles, the profile and the time of drug release [7]. Among several diseases, gastrointestinal candidiasis (GIC) [8] was chosen to formulate and optimize a medicinal product taking into consideration the enhancement of the bioavailability of local effect.

Application of pellets in this therapy offers even more advantages. They are suitable to optimize drug release by their particle size, coating thickness or material.

Pellets among multiparticulate dosage forms offer several advantages generally in the therapy related to safety and effectiveness of the medicinal product such as individual reproducibility of gastric emptying, more regular absorption, increasingly stable, predictable plasma levels and a reduced risk of high concentrations [9,10]. This basic concept of multiple-unit systems is the fact that the dose of the active ingredient is released by the individual subunits, and the functionality of the entire dose depends on the quality of the subunits [11]. Pellets are suitable for further processing in order to optimize drug release by combining different particle size fractions and coating thickness [12] in capsules or compressing them into tablet.

Manufacturing of pellets requires specialized equipments, technologies and excipients. Pellets are usually prepared by wet agglomeration of fine powders of active ingredient and excipients into spherical units in closed granulating systems, i.e. in rotor-fluid granulators or high-shear mixers [13]. To produce pellets in a high shear mixer, the process involves distinct phases: homogenization of powders, granulation, spheronization and drying. The primer nucleus of future pellets is formed by binder spraying and dispersing during the agitation. Being a multivariate process, it is important to identify and control the process variables, i.e. the appropriate agitation prevents the development of too large particles [14,15,76]. Since

agglomerates undergo densification as mixing and spraying, the process time is expected as a critical parameter influencing quality of pellets.

Although various experiments were drawn up to investigate the effect of the formulation variables on the physical characteristics of pellets, only a few reports can be found in the pharmaceutical literature investigating the large number of process variables together during the pelletization concerning both the physical properties of granules and the drug release profile of the dosage form [16].

Modelling the effect of process variables with factorial designs and analysis of the response surfaces is a powerful, efficient and systematic tool that shortens the time required for the development of pharmaceutical dosage forms and improves research and development work [20].

The objective of the dissertation is to offer an optimized pharmaceutical preparation for the therapy of GIC containing *nystatin* to achieve a prolonged site-specific antifungal treatment using multiparticulate dosage form and special bioadhesive excipients based on preliminary examinations carried out on micropellets with model drug incorporated.

2. Aims

Aims of this research work are:

- determination of significant process variables and their effect of high-shear pelletization,
- application of the measurement of diffuse reflectance spectra as a possibility for fast in-process control during the pelletization process,
- application of optimized process variables in order to produce micropellets with specific physical characters for an optimized GIC therapy,
- application of Microbiologically Detected Dissolution (MDD) technique based on direct bioautography in order to determine the dissolution kinetics of antifungal substances,
- comparison of the MDD with other analytical method,
- optimizing the biopharmaceutical characters of micropellets for the antifungal action,
- recommendation of the manufacturing method and ingredients for a successful GIC therapy.

3. Literature survey

The literature survey of the thesis contains two parts. The first is concerned with the technological manufacture and optimization, the second part handles the therapeutic importance of locally acting micropellets.

Definition of pellets is not uniform, sometimes they are discussed together with granules and often the terms pellet-micropellet are not distinguished. Their preparation can be carried out in many ways with similarities to the preparation of granules [21]. According to the literature there are a few fix points which can characterize the pellet dosage form as spherical particles with almost smooth surface and compact texture independently to the method of preparation. If their size is below 1 mm, the term “micropellet”, between 1 and 2 mm, the term ”minipellet” can be used.

According to the structure, as seen on Fig. 1 we can distinguish pellets containing the API in the

1. matrix and in the
2. coating.

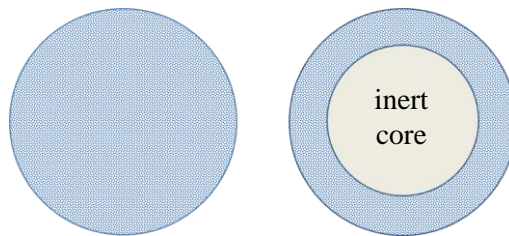


Figure 1. Basic types of pellets

(matrix pellet containing API on the left; inert pellet core with layer containing the API on the right)

Pellets have several pharmaceutical technological advantages, such as excellent flowability, easily optimizable particle size distribution, good mechanical stability, abrasion-resistant structure and optimizable coating due to the regular, uniform, smooth surface [13].

3.1. Interaction between particles, distribution of binder liquid

Interaction between solid particles during granulation was first scientifically investigated by *Rumpf* in the 50s [23]. In his work the following forces were listed:

1. attrition forces – gravitational force, magnetic force, electrostatic force or the van der Waal force play less role in the interactions between particles, than capillary forces,
2. solid bridges – they are developing during the formation of inorganic bonds, chemical reactions, crystallisation and melting phenomena,
3. shape closing bridges – they are developing due to the different shape and size of particles during pelletization getting into physical contact to each other,
4. liquid bridges – they are forming due to capillary forces which ensures the cohesion of particles and decrease the attrition forces.

Newitt and *Conway-Jones* distinguished four phases during the development of spherical particles according to the distribution of the binder liquid: the pendular state with liquid bridges, the funicular state in which the amount of liquid bridges increases capillary state and the droplet state [24].

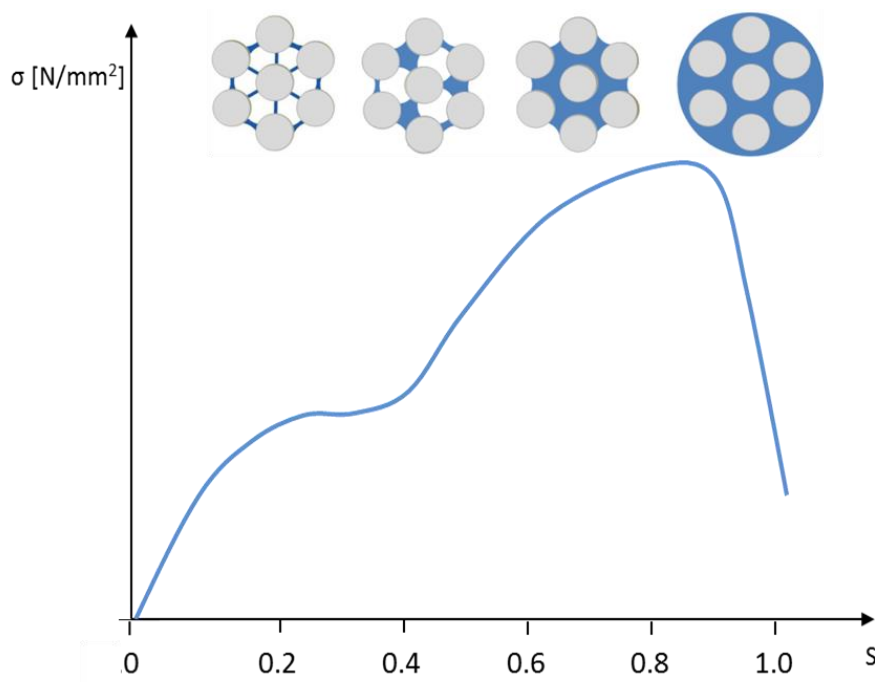


Figure 2. Stages of wetting (S means the liquid saturation level) and tensile strength (σ) during granulation

During pelletization right before the addition of any liquid small size particle-aggregates can be observed due to the secondary attrition forces. After the beginning of addition of liquid first drops start to connect the primary particles at the contact points. At the next, funicular stage, the liquid bridges may reach each other and more than two primary particles can be connected via this liquid bridge. Gaps are also started to be filled with liquid at this stage. At the next stage the structure of the pellet is formed and due to the capillary state the liquid added to the system is absorbed by the aggregated structure. The mechanical stability of the pellet is the highest at this point. Increasing the amount of the added liquid the droplet state can be reached, when the structure weakens and the system turns into paste or suspension.

Basically we can distinguish two types of binder liquid additions:

1. the size of the liquid drop is bigger than the size of the primary particle (drop addition),
2. the size of the liquid drop is smaller than the size of the primary particle (spray addition).

During the wetting of the powder mixture the contact angle (Θ) is the most important physical property which describes the wetting mechanism on the solid/liquid/gas boundary surface, which is the angle of solid/liquid and liquid/gas boundary surface.

We can distinguish:

1. contact wetting ($\Theta > 0^\circ$),
2. film wetting ($\Theta = 0^\circ$).

In case of $\Theta < 90^\circ$ we can state, that the substance is lyophilic, in case of $\Theta > 90^\circ$ it is lyophobic. After the equilibrium of solid/liquid/gas phases the relationship between the surface tension and the contact angle can be expressed by the *Young-Dupré* equation:

$$\gamma^{sv} - \gamma^{sl} - \gamma^{lv} \cos \Theta = 0 \quad (1)$$

| | |
|---------------|------------------------------|
| γ^{sv} | solid/gas surface tension |
| γ^{sl} | solid/liquid surface tension |
| γ^{lv} | liquid/gas surface tension |
| Θ | contact angle |

Another way of characterisation of the wetting is the *Washburn*-test, which is based on the penetration of a liquid into a column filled with particles due to capillary forces. This phenomenon can be described by the following equation:

$$h_e - \frac{2\gamma^{lv} \cos\theta}{\rho g R} = 0 \quad (2)$$

| | |
|--------------------------|---|
| h_e | height of the liquid after the equilibrium |
| R | average radius of capillaries in the particle agglomerate |
| ρ | density of the liquid |
| g | gravitational force |
| $\gamma^{lv} \cos\theta$ | adhesion tension |

3.2. Particle growth and attrition mechanism during pelletization

During pelletization the balance of particle growth and attrition mechanisms is very fundamental. We can distinguish four types of these mechanisms:

1. Nucleation – is the first step during particle growth, when primary particles are getting into contact to each other and stick together in the presence of the binder liquid forming a nucleus.
2. Coalescence – due to the collision of particles bigger aggregates are formed.
3. Layering – also called as „balling”, when a larger amount of primary particles stick on the surface of a bigger aggregate due to liquid addition.
4. Breakage – there are more mechanisms for the breakage of granules/pellets:
 - a. crushing – during which smaller granules or pellets crush and get onto the surface of bigger particles. There are several mechanisms of crushing:
 - i. shattering,
 - ii. fragmentation,

- iii. abrasion,
- b. abrasion transfer – during which the material transfer occurs between two colliding particles, while both particles stay intact.

These mechanisms are often described mathematically by different models according to different steps of pellet formation. Strength of liquid bridge between two colliding particles determines whether they stay intact or attach together. The greatest force which depends on the relative amount between two particles comparing to their volume was first described by *Rumpf* [23]:

$$F_{cap} = \alpha \gamma_l d_p \quad (3)$$

$1.9 < \alpha < \pi$ coefficient depending on the amount of moisture

γ_l surface tension of the liquid

d_p diameter of the particle

Rumpf described another relationship for the breakage of granules, which includes the particles tensile strength (σ_t) in funicular or capillar state:

$$\sigma_t = C \cdot S \cdot \frac{1 - \varepsilon}{\varepsilon} \cdot \frac{\gamma_l}{d_{pp}} \cdot \cos \Theta \quad (4)$$

C coordination number dependent from the shape of the particle

S liquid saturation of the granule

ε intragranular porosity

d_{pp} diameter of the primary particle

Θ contact angle

Ouchiyama and *Tanaka* determined a model which can be used to calculate the critical diameter (d_c) above which there is no coalescence [25]:

$$dc = c \cdot \left(K^{3/2} \cdot \sigma_t \right)^a \quad (5)$$

a and c constants

K deformation constant

σ_t tensile strength of the granule

The ' K ' deformation constant can be described as the ratio of the contact surface (A) and the compaction force (F):

$$K = \frac{A}{F} \quad (6)$$

Kristensen et al completed *Ouchiyama* and *Tanaka*'s model to calculate the tensile strength of the granule particles and stated that granule particles must reach a minimal mechanical stability for the coalescence [26].

Ennis et al recognized, that the viscosity of the liquid significantly influences the cohesion force of the liquid bridge, thus an agglomeration model was developed for the dynamic liquid bridge [28]. Depending on the kinetic energy during the collision of particles the energy spread across the system is used at coalescence or the reflexion of particles. To describe this system *Ennis* et al introduced the dimensionless viscous Stokes number:

$$St_v = \frac{8\rho_p v_0 r}{9\eta} \quad (7)$$

| | |
|----------|---|
| ρ_p | density of the pellet/granule |
| v_0 | relative velocity between two particles |
| r | radius of the pellet/granule |
| η | viscosity of the binder liquid |

The viscous Stokes number is the ratio of two colliding particle's energy and the spreading of energy in a viscous binding liquid [29]. In case of a high-shear granulator the velocity of the collision is in direct proportion to the impeller rotation speed (v_{imo}):

$$v_{imo} = \pi ND \quad (8)$$

| | |
|-----|----------------------------------|
| N | rotating speed of the impeller |
| D | diameter of the granulation bowl |

Since in case of collision of two particles they lose kinetic energy, the velocity before the collision (v_0) is higher than the velocity after the collision (v).

Coalescence occurs when the viscous Stokes number (St_v) is smaller than its critical value (St_v^*):

$$St_v^* = \left(1 + \frac{1}{e}\right) \ln\left(\frac{h}{h_a}\right) \quad (9)$$

| | |
|-------|---|
| e | rearrangement coefficient, which can be calculated from the difference of velocity before and after the collision |
| h | thickness of the liquid layer on the surface of the pellet |
| h_a | surface roughness (diameter of the primary particles is also ' h_a ') |

According to the theory above there are three cases regarding the values St_v and St_v^* :

1. $St_v \ll St_v^*$ - in this case all collisions are successful
2. $St_v = St_v^*$ - some collisions are successful
3. $St_v \gg St_v^*$ - none of the collisions are successful

From the expressions above we can state, that the collision of the particles and growth by coalescence has higher probability at low particle density, low impeller speed, small particle size, high viscosity liquid binder, small rearrangement coefficient, thick surface liquid layer and smooth particle surface. Since these variables usually change in function of time, above calculations can only be used for retrospective studies.

3.3. Operation of pelletization

Similarly to the granules there are three main types of operations of pelletization:

1. **Solvent pelletization** – the applied liquid dissolves totally or partially one or more components of the powder mixture. During the addition of the liquid a saturated solution develops on the surface of the particles which binds them together. After the evaporation of the solvent the dissolved component gathers on the surface of the pellet and crystallizes, forming a thick coating (Fig.3.) [21].

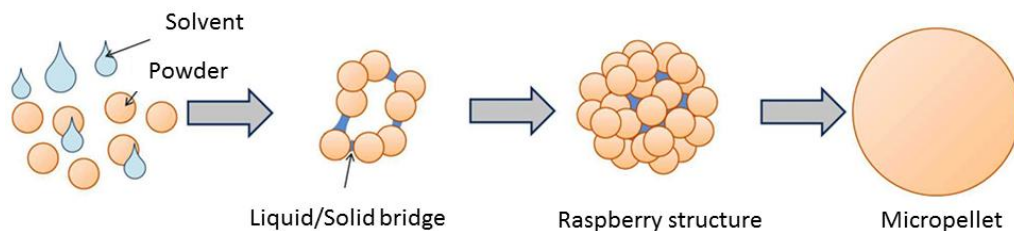


Figure 3. Mechanism of pelletizing with solvent

2. **Binder pelletization** – usually high molecular weight polymers are used. The powder mixture is usually wetted by the proper amount of binder liquid and then it is kneaded. The binder material also can be added in its powder form, but these pellets' mechanical properties are usually poor (Fig.4.) [21].

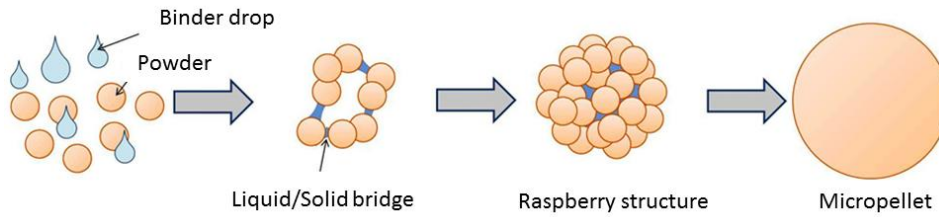


Figure 4. Mechanism of pelletizing with binding agent

- Sinter pelletization** – in this case one or more components of the powder mixture has a lower melting point (usually high molecular weight macrogol). Heating the mixture partial melting occurs. Spray drying or freeze drying this mixture result almost perfectly spherical pellets (Fig.5.) [21].

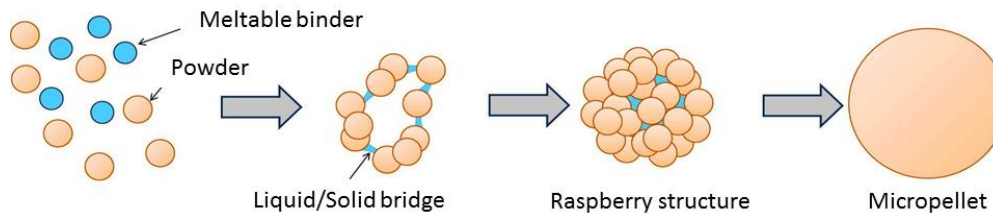


Figure 5. Mechanism of pelletizing with sintering

In order to carry out pelletizing, several procedures are available, which will be discussed in the following chapters.

3.3.1. Mixing method

This is the simplest way of pelletisation. This method usually results heterogeneous particle size distribution. During this method the powder mixture and the liquid binder both are placed into a rotating caldron, where the pellets are formed [13].

3.3.2. Rotary disk method

The powder mixture is placed on the surface of a rotating flat disk or a conical body, while the binder liquid is added from the centre of the rotating axis. Developing particles roll to the edge of the rotating disk due to the centrifugal force, during which they gain their spherical shape. Using this method spheronization of preliminary prepared granules can also be carried out (Fig.6.).



Figure 6. Rotary disk pelletizing equipment [77]

3.3.3. Extrusion-spheronization method

This is one of the most commonly used pellet preparation method [27]. Powder components are kneaded with the liquid, then the wet mass is extruded through a 0.5-2.0 mm diameter hole size disk. After this step the plastic and wet extrudate is spheronized (Fig.7.) [30].



Figure 7. Extruder during operation [77]

3.3.4. Roto-fluid method

Applying fluid-bed granulation, spheronization and drying is carried out in one complex step. There is a rotating disk at the bottom of the machine with a conical body in the centre (Fig. 8.). Due to the fluid air, the rotating disk and the conical body particles circulate around the wall of the working area and roll on the surface of the disk. The liquid is added towards the centre of the working space spraying the liquid to the rotational direction. Reaching the proper particle size the liquid addition is stopped and from this point only spheronization and drying is carried out. Roto-fluid pelletization is one of the most power consuming and expensive methods, its advantage is the high productivity and the one-step production [21].

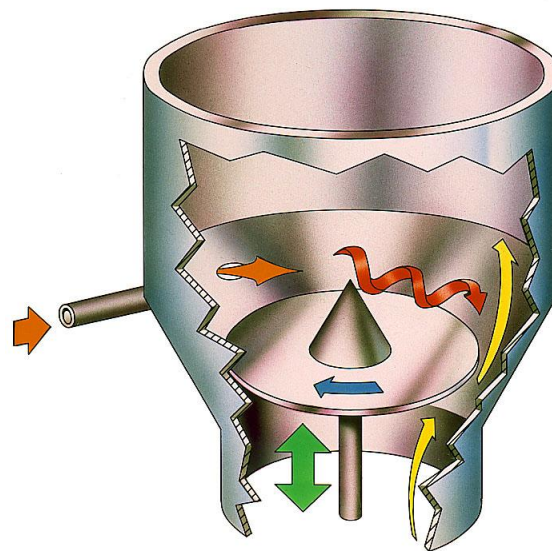


Figure 8. Operation of roto-fluid machine [77]

3.3.5. Spray drying and freeze drying

API is dispersed in the vehicle's solution, and then it is sprayed. Perfectly spherical droplets formed during this preparation are then dried by hot or cold air [21].

3.3.6. High-shear pelletization

This method unifies the main steps of the classic wet granulation (homogenization, wetting, kneading and particle forming) and the spheronization. The production is carried out in one working space similarly to the fluidisation in one complex step (Fig. 9.). During high-shear granulation intense mixing of the components and the presence of the shearing forces results the smooth and compact spherical particles. The mechanical parameters of the end-product depend on the operation variables. Spray or drop form of liquid is immediately dispersed due to the high rotation speed of mixer elements, thus reaching a quick and perfect wetting. Main mixer elements consists the impeller and the chopper. The impeller is at the bottom of the working space reaching rotation speed of 500-2000 rpm. The impeller moves the mass around the working space and in radial direction outwards from the centre to the wall. The mass produces a whirling movement and continuously falls back towards the centre. Chopper blades can be placed at the bottom, top or tangentially to the rotation axis of the impeller. This mixer element is composed of more smaller, thinner blades (3-6), which enhance the shearing forces during the production. Their speed also varies between 500-2000 rpm. Pellets produced in the high-shear machine can be dried by microwave or heating double-jacket as well. The production method is extremely quick, there is low risk of contamination due to the closed working area. Choosing the proper operation variables and applying the proper excipients almost all pharmaceutical technological and biopharmaceutical parameters can be optimized and controlled [13].

Most important variables during high-shear production related to the equipment:

1. mixing bowl
 - a. shape
 - b. size
 - c. material
2. impeller
 - a. shape
 - b. size
 - c. speed
3. chopper
 - a. shape
 - b. size
 - c. speed
4. temperature of the working space
5. operation time

Most important variables during high-shear production related to the material are:

1. powder composition (particle size distribution, physical properties)
2. weight
3. liquid binder
 - a. viscosity
 - b. density
 - c. amount
 - d. dosing speed
 - e. dosing method

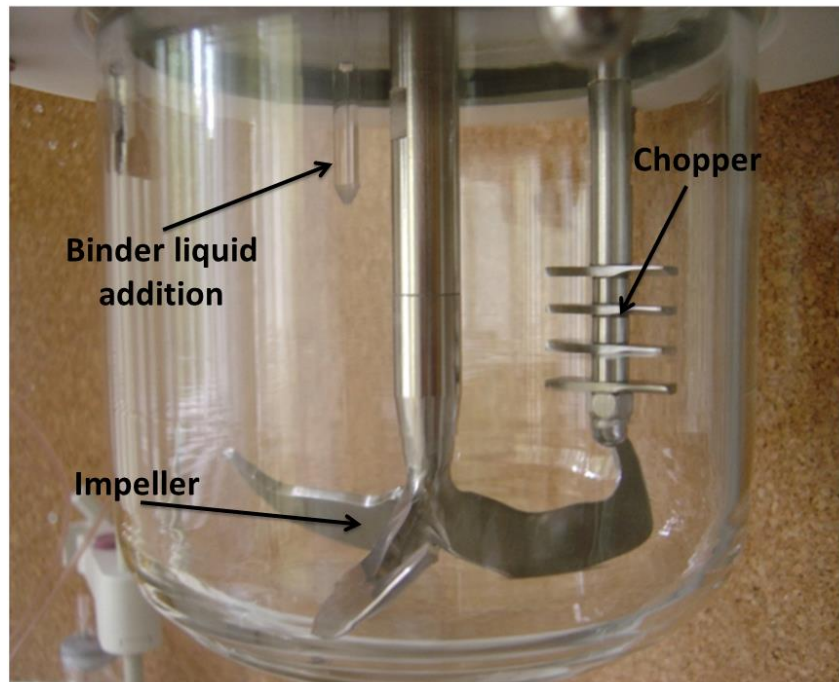


Figure 9. Lab-scale high shear granulator (Pro-C-epT 4M8, Belgium, Zelzate)

3.3.6.1. Forces during high-shear pelletization

During pelletization presence and equilibrium of integration and reduction effects leads to the formation of pellets, which are based on the following forces:

- gravitational force
- acceleration force
- centrifugal force
- resistance of the pelletizing bowl
- fluid effects developed by the impeller

For the characterisation of the forces effecting the preparation, the tip speed of the impeller is commonly used, which is directly proportional to its shearing force. The perimetric speed is responsible for the movement of the wet mass. This value can be calculated by the following expression:

$$v_t = v_f 2 \pi r \quad (10)$$

| | |
|-------|--|
| v_t | velocity of the tip of the impeller |
| v_f | speed of the rotor of the impeller (rpm) |
| r | radius of the circle done by the tip of the impeller |

The Froude number describes the forces affecting to the wet mass resulting its compaction, which is carried out by the impeller. The *Froude* number is a dimensionless value.

$$Fr = \frac{v^2 r}{G} \quad (11)$$

| | |
|------|--|
| Fr | Froude number |
| v | speed of the impeller |
| r | radius of the circle done by the tip of the impeller |
| G | acceleration of gravity |

At smaller, laboratory production scale the Froude number is usually higher, than in industrial scale. The higher number means bigger pellet size, more compact structure, which can result the cohesion of the particles to the pelletizing bowl [33].

3.3.6.2. Determination of end-point of high-shear pelletization

Critical point of the high-shear pelletization is the determination of the end-point of the production. The end-point is usually determined by the technologist according to the particle size, the particle size distribution, density, and the powder rheology. Instrumented high-shear machines have several parameters which are observed in order to forecast and determine the optimal end-point [34].

Most important methods include:

- measurement of power consumption,
- measurement of the impeller torque,
- other methods based on the measurement of the impeller torque,
- alternative measurement methods.

3.3.6.2.1. Measurement of power consumption

One of the most commonly used methods is the measurement of the power consumption of the impeller. Scientific literature several times reported that the increase of the pellet size has close correlation to the increasing power consumption. This correlation is not linear, but it is characteristic and reproducible to the definite powder composition [35].

3.3.6.2.2. Measurement of the impeller torque

The second most commonly used method is the measurement of the impeller torque, which has good correlation to the previously mentioned method, since sometimes it is recommended to use the more complex measurement of the impeller torque due to insensitivities in the power consumption profile in case of definite weight of mass or other specific parameters. The profile of the impeller torque divides the pellet formation process into five phases. In the first phase the powder is moistened without forming liquid bridges. In the second phase liquid bridges are formed between the particles and first granules are formed. Formation of coarse

agglomerates could be observed in the third phase and in the fourth phase large areas are filled with liquid. In the fifth phase when the liquid saturation equals 100%, the system becomes a suspension [35]. The end-point of the pelletization is usually during the fourth phase.

3.3.6.2.3. Other methods based on the measurement of impeller torque

- **Torque rheometer method** – the third most commonly used method, which also provides information on rheological properties [38].
- **Torque reaction force method** – applies Newton's third law of action-reaction. During the measurement the rotor tries to move against the rotational direction which develops forces inside the engine, which can be detected and used for the end-point determination [35].

3.3.6.2.4. Alternative measurement methods

There are several other measurement methods supplementing the lacks of the methods mentioned above:

- **Application of NIR sensor** – this method is based on the moisture changes of the particles. Its disadvantage is that the sensor can only detect the moisture on the surface of the wet mass [39].
- **Focused Beam Reflectance Measurement (FBMR)** – the method is based on the particle size determination. This method cannot be used for end-point determination alone, but it can be a perfect supplement of other methods [40].
- **Acoustic sensor measurement** – one of the oldest methods of the end-point determination which can be used alone and as a supplementing tool as well. Development of the technology in recent years and modern analysis softwares provide more potential to this method [31].

3.4. Biopharmaceutical background

Gastrointestinal candidiasis (GIC) often occurs in patients suffering from immunosuppression (e.g. related to HIV infection), but many researchers found GIC also in non-immuno suppressed humans. GIC belongs to one of the most discussed diseases, since it is still undecided whether it can cause systemic symptoms or not. Researches, however, indicate GIC diseases may be more prevalent than it is supposed. Several antifungal pharmaceutical ingredients are considered to be effective in the therapy of GIC as listed in Table I [43].

Table I. BCS classification of antifungal agents used in candidiasis

| BCS Class | Antifungal agent | Biopharmaceutical properties |
|-----------|-----------------------------------|------------------------------------|
| 1 | - | high solubility, high permeability |
| 2 | <i>clotrimazole, itraconazole</i> | low solubility, high permeability |
| 3 | <i>fluconazole, capsosungin</i> | high solubility, low permeability |
| 4 | <i>amphotericin B, nystatin</i> | low solubility, low permeability |

Clotrimazole (Fig. 10.) belongs to the group of imidazoles, it is applied in 10 mg troches 5 times a day in mucosal candidiasis. According to the Ph. Eur. 8. it is white or pale yellow crystalline powder. It is practically insoluble in water; soluble in alcohol, in acetone, in chloroform, and in methyl alcohol [44].

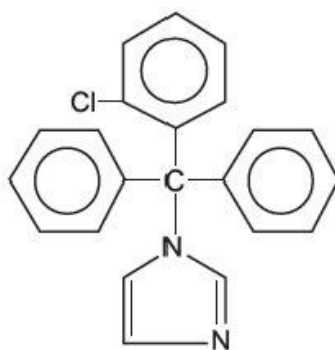


Figure 10. Structural formula of *clotrimazole*, 1-(α -2-Chlorotriptyl)imidazole

Itraconazole (Fig. 11.) is a triazole antifungal ingredient applied in oral solution 200 mg/day. This substance is a white powder, insoluble in water; very slightly soluble in alcohol; freely soluble in dichloromethane; sparingly soluble in tetrahydrofuran [44].

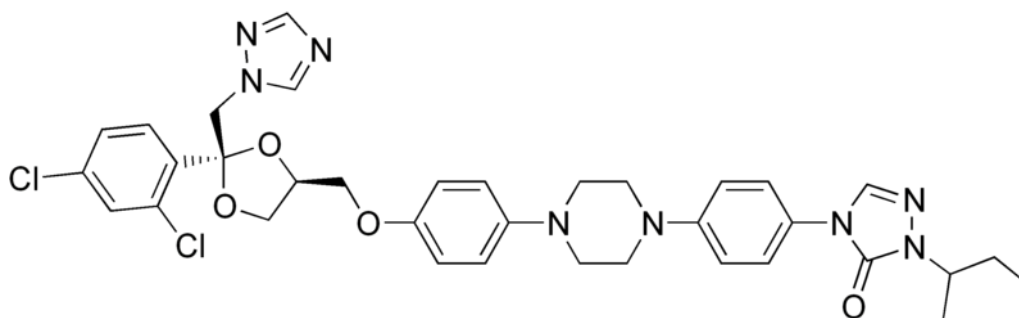


Figure 11. Structural formula of *itraconazole*, (±)-2-sec-Butyl-4-[4-(4-{4-[(2*R**,4*S**)-2-(2,4-dichlorophenyl)-2-(1*H*-1,2,4-triazol-1-ylmethyl)-1,3-dioxolan-4-ylmethoxy]phenyl}-piperazin-1-yl)phenyl]-2,4-dihydro-1,2,4-triazol-3-one

Fluconazole (Fig. 12.) is also a triazole antifungal ingredient applied in 100-200 mg. It is a white or almost white, hygroscopic, crystalline powder, slightly soluble in water; freely soluble in methyl alcohol; soluble in acetone [44].

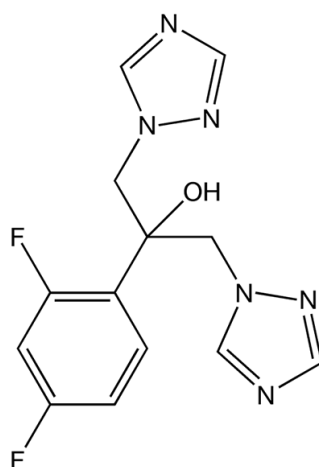


Figure 12. Structural formula of *fluconazole*, 2-(2,4-Difluorophenyl)-1,3-bis(1*H*-1,2,4-triazol-1-yl)propan-2-ol

Caspofungin (Fig. 13.) is a β -3-glucan synthase inhibitor applied in 50 mg i.v. dose [44].

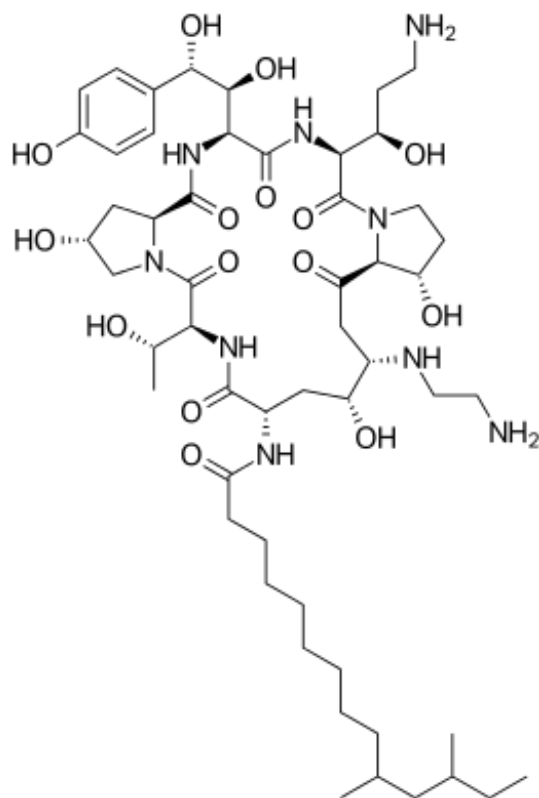


Figure 13. Structural formula of *caspofungin*, (4R,5S)-5-[(2-Aminoethyl)amino]-N2-(10,12-dimethyltetradecanoyl)-4-hydroxy-L-ornithyl-L-threonyl-trans-4-hydroxy-L-prolyl-(S)-4-hydroxy-4-(p-hydroxyphenyl)-L-threonyl-threo-3-hydroxy-L-ornithyl-trans-3-hydroxy-L-proline cyclic (6→1)-peptide diacetate

Amphotericin B (Fig. 14.) yellow or orange powder, which is a mixture of polyene antifungal ingredients, produced by the growth of certain strains of *Streptomyces nodosus*. It is practically insoluble in water and in alcohol; soluble in dimethyl sulfoxide and in propylene glycol; slightly soluble in dimethylformamide; very slightly soluble in methyl alcohol [44]. 100mg/ml oral suspension is also applied, though due to its absorption severe side effects might occur as well as in case of other effective antimicrobial substances, since the high concentration of the applied antifungal agents may develop severe side effects [45].

$C_{47}H_{73}NO_{17} = 924.1$

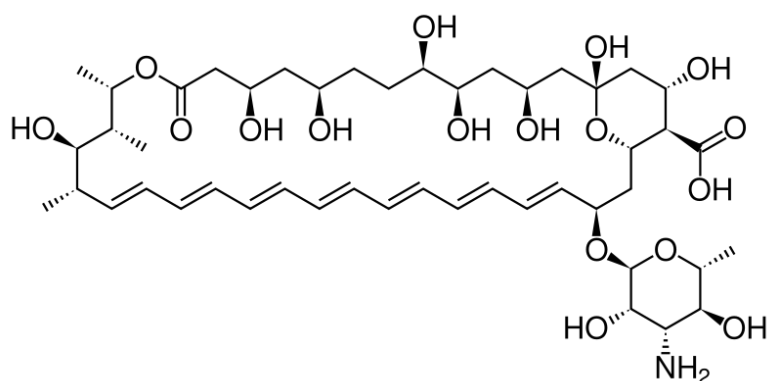


Figure 14. Structural formula of *amphotericin B*, (1*R*,3*S*,5*R*,6*R*,9*R*,11*R*,15*S*,16*R*,17*R*,18*S*,19*E*,21*E*, 23*E*,25*E*,27*E*,29*E*,31*E*,33*R*,35*S*,36*R*,37*S*)- 33-[(3-amino- 3,6-dideoxy- β -D-mannopyranosyl)oxy]-1,3,5,6,9,11,17,37-octahydroxy- 15,16,18-trimethyl- 13-oxo- 14,39-dioxabicyclo [33.3.1] nonatriaconta-19,21,23,25,27,29,31-heptaene- 36-carboxylic acid

Pharmaceutical character of *nystatin* will be summarized later in chapter 4.1.1. Its effect is based on the topical action and the contact time with the mucous membrane, thus the formulation should adhere to the affected area as long as possible, however available dosage forms are unable to achieve an optimized effect, lacking the specialities of the adequate topical treatment. To reach this aim, mucoadhesive materials are needed to be added. Application of mucoadhesive polymers in the formulation, such as the anionic carbomer (CPL) and the non-ionic hydroxyethylcellulose (HEC) is a possible method for the targeted mucosal drug delivery which has been introduced to the pharmaceuticals in the late 1960s [48].

In our study after preliminary examinations of high-shear granulation, *nystatin* was chosen as one of the most adequate API for the treatment of GIC due to its preferential properties [43]. Micropellets containing *nystatin* with increased specific surface were produced according to an experimental design containing bioadhesive excipients, which can prolong the contact time with the mucous membranes. The pellet size and the proportion of bioadhesive substances (carbopol®/hydroxyethylcellulose) were taken into consideration as variables affecting the therapy [51].

During the evaluation, in vitro spectrophotometrical, microbiological dissolution, ex vivo bioadhesion and swelling tests were carried out.

Effectiveness of the produced medicament samples was evaluated by the determination of the drug release [52]. Developing possibilities of *nystatin* determination methods are continuing intensively, since classic UV analytical methods in the pharmaceutical practice are not suitable to follow exact changes of antifungal activity of *nystatin* [53]. UV spectrum of *nystatin* demonstrates three main local maxima at 290, 306 and 318 nm which are only reliable at the same molecular state. Micellar structure of the polyene *nystatin* can lead to differences in the UV spectrum [54]. Numerous colour reactions were also tested, but there was no confirmed correlation with the biological activity [55]. A generalized assumption was later published regarding the lack of relationship for all polyene antibiotics between the UV spectrophotometric assay and the biological activity, which eventuated to include an agar diffusion method for the quantitative assay of *nystatin* in the Ph. Eur. 5. However, the agar diffusion method is sometimes time, cost and power consuming especially in case of large quantity of samples. Application of thin layer chromatography (TLC) based direct bioautography during the drug dissolution tests, microbiologically detected dissolution (MDD) can be carried out [56]. The MDD does not need strict sterile conditions and it is almost 100 times more sensitive than the agar diffusion method. Novel approach to enhance the UV spectrophotometric determination and to achieve better correlation is the application of the third-derivative spectrophotometric evaluation, which was applied in our experiments. The objective of the present study is to offer an optimized drug formulation by revealing the relationship between average pellet size, CPL and HEC content and optimized drug release to achieve a site-specific antifungal therapy.

4. Materials and Methods

4.1. Materials

4.1.1. Nystatin

The polyene antifungal antibiotic *nystatin* (Fig. 15.) (BCS class IV.) is one of the most important active agents in the site-specific treatment of the candidiasis [46], as it was reported by several clinical researches. *Nystatin* is a yellow or slightly brownish hygroscopic substance obtained by fermentation using the ATCC 11455 strain of *Streptomyces noursei* [44]. *Nystatin* is very poorly absorbed from the gastrointestinal tract, therefore the development of side effects is suppressed. It is excreted almost entirely in the faeces.

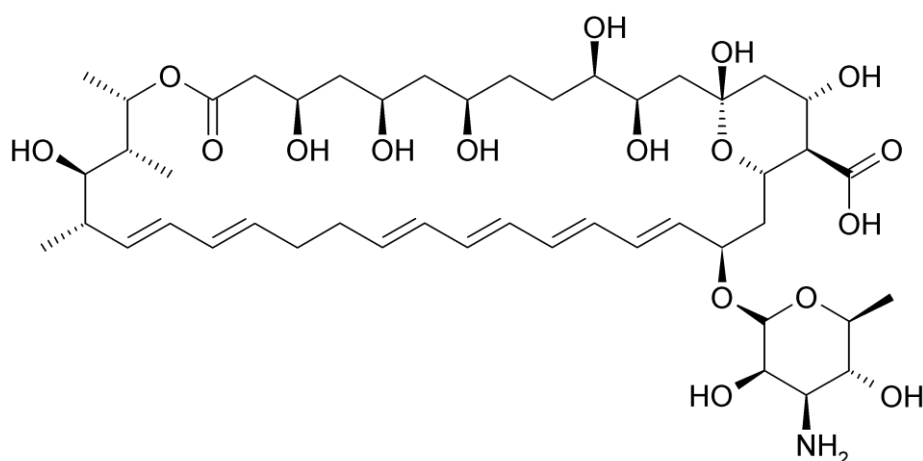


Figure 15. Structure of *nystatin*, (1*S*,3*R*,4*R*,7*R*,9*R*,11*R*,15*S*,16*R*,17*R*,18*S*,19*E*,21*E*,25*E*,27*E*,29*E*,31*E*,33*R*,35*S*,36*R*,37*S*)-33-[(3-amino-3,6-dideoxy- β -L-mannopyranosyl)oxy]-1,3,4,7,9,11,17,37-octahydroxy-15, 16,18-trimethyl-13-oxo-14, 39-dioxabicyclo[33.3.1]nonatriaconta-19, 21,25,27,29,31-hexaene-36-carboxylic acid

4.1.2. Pharmaceutical excipients

4.1.2.1. Microcrystalline cellulose

Microcrystalline cellulose is purified, partially depolymerized cellulose that occurs as a white, odourless, tasteless, crystalline powder composed of porous particles. Microcrystalline cellulose is widely used in pharmaceuticals, primarily as a binder/diluent in oral tablet and

capsule formulations where it is used in both wet-granulation and direct-compression processes [36]. In our experiments Avicel PH 101 and Avicel PH 105 were used.

4.1.2.2. α -lactose-monohydrate

Lactose occurs as white to off-white crystalline particles or powder. It is odourless and slightly sweet-tasting; the lactose is approximately 20% as sweet as sucrose. This excipient is widely used as a filler or diluent in tablets and capsules [36].

4.1.2.3. Ethylcellulose

Ethylcellulose (EC) is a tasteless, free-flowing, white powder. Ethylcellulose is widely used in oral and topical pharmaceutical formulations. The main use of ethylcellulose in oral formulations is as a hydrophobic coating agent for tablets and granules. Ethylcellulose coatings are used to modify the release of a drug) to mask an unpleasant taste, or to improve the stability of a formulation; for example, where granules are coated with ethylcellulose to inhibit oxidation. Modified release tablet formulations may also be produced using ethylcellulose as a matrix former [36].

4.1.2.4. Hydroxyethylcellulose

Hydroxyethylcellulose (HEC) occurs as a light tan or cream to white colored, odorless and tasteless, hygroscopic powder. Hydroxyethylcellulose is a non-ionic, water-soluble polymer widely used in pharmaceutical formulations, primarily used as a thickening agent in ophthalmic and topical formulations. It is also used as a binder and film-coating agent for tablets as well as an excipient for its bioadhesive properties [36].

4.1.2.5. Carbomer

Carbomers (CPL) are white-colored, acidic, hygroscopic powders with a slight characteristic odour. Carbomers are synthetic high-molecular-weight polymers of acrylic acid that are cross-linked with either allyl sucrose or allyl ethers of pentaerythritol. They are mainly used in liquid or semisolid pharmaceutical formulations as suspending or viscosity-increasing agents.

Formulations include creams, gels, and ointments for use in ophthalmic, rectal and topical preparations. It is also used as a bioadhesive material in oral preparations [36].

4.2. Methods

4.2.1. Design of experiments

Design, operation and control of pharmaceutical technological systems are based on information and their processing. Understanding of procedures is carried out by data mining, which means knowledge discovery from a database. Data mining is a scientific action, which aims at discovery of particular phenomena and procedures by data management and search and analysis of their correlations.

Afterwards discovery of procedures (process analysis) will take place the control of procedure, which can only be efficient, if factors can be determined, which are influencing quality parameters. The factors can be grouped accordingly how extent and in which way are able to effect on particular parameters.

One of the most important tasks of experimental design is the optimization of a preparation, which can be defined as search of the best and most favourable values of a phenomenon in order to create the necessary technological conditions. Size of manufacture batch, manufacturing time and particular operation parameters can also be obtained by optimization of parameters [58].

With the usage of factorial experimental design, few numbers of experiments are enough to explore the correlation between independent and dependent variables. Requirements of chosen parameters and factors are:

- controllability,
- accuracy,
- factor has to be unambiguous and directed to the particular object,
- independence between factors.

The experimental design (ED, or Design of Experiment, DOE) means plan or design containing settings and sequence, which has to be compiled even before beginning of experiment. This is an effective method, which allows planning and analysis of experiments,

objective evaluation of obtained result, conclusion, after which follow the steps for optimization of particular process.

Full factorial experimental design is regarded if all possible factor level combination and fractional factorial experiments are performed. If just a part of the full, partial factor design is carried out. Latter one can significantly reduce the necessary number of experiments, which should be performed.

The linear model

for two factors (x_1 and x_2):

$$Y = b_o + b_1x_1 + b_2x_2 + b_{12}x_1x_2 \quad (12)$$

b coefficient

x_1x_2 interactions

for three factors (x_1, x_2 and x_3):

$$Y = b_o + b_1x_1 + b_2x_2 + b_3x_3 + b_{12}x_1x_2 + b_{13}x_1x_3 + b_{23}x_2x_3 + b_{123}x_1x_2x_3 \quad (13)$$

b coefficient

$x_1x_2, x_1x_3, x_2x_3, x_1x_2x_3$ interactions

Mathematic model determined experimentally is appropriate to describe or characterize an examined system, if it meets with the criteria of adequacy. Namely there is no significant difference between output of system calculated according to computer and output of actual system.

Optimization can be performed by applying the gradient descent method developed by *Box and Wilson*. The principal of this method is that in order to determine the optimum, simultaneous change of significant factors is required [59].

4.2.2. Preliminary studies for high-shear pelletization

Among the available methods of preparation high-shear granulation was chosen to produce pellets. In order to determine significant process parameters of high-shear granulation, pellets were prepared containing anhydrous theophylline as model drug, α -lactose monohydrate, microcrystalline cellulose and ethylcellulose. Quality of all materials used in the experiments was Ph. Eur. 5. The powders were loaded into the bowl and premixed for 3 min.

During the pelletization the amount of the purified water used as granulation liquid was the amount of 45% calculated on the loaded mass. The binder flow time was kept constant at 5 minutes.

After production, pellets were dried to constant weight at 35°C, and stored at 25 °C, 60% RH in closed containers until their evaluation.

The high shear pelletization process was performed in a Pro-C-epT 4M8 granulator (Zelzate, Belgium). During the production two process variables were chosen to be investigated defined as factors [59]:

- impeller speed (x_1),
- binder flow rate (x_2).

Chopper speed was constant kept at 2000 rpm. An experimental design was carried out to reduce the number of experiments needed to obtain the highest amount of information on product and the effect of manufacturing process variables. The trials were carried out in triplicate in a randomized order. The variation intervals of independent variables and their coded levels are detailed in Table II. First, to find the most powerful process parameters, a 3-level face-centred central composite experimental design was conducted assuming a second order polynomial model according to the matrix demonstrated by Table III. The highest order of interaction (x_1x_2) was chosen as design generator to minimize the alias of coefficients through the defining contrast.

Table II. Independent process variables: factors and their coded levels

| Factors | Variation intervals | | |
|----------------------------|---------------------|-------------|---------------|
| | Low (- 1) | Base (0) | High (+ 1) |
| x_1 impeller speed (rpm) | 500 | 750 | 1000 |
| x_2 binder flow (ml/min) | 8 | 10 | 12 |

Table III. 2-factor, 3-level face centred central composite experimental design matrix for the pelletization

| Trial | Controlled factor | |
|-------|-------------------------------------|-------------------------------------|
| | x_1 Impeller speed (rpm) | x_2 Binder flow (ml/min) |
| 1 | 1000 | 12 |
| 2 | 500 | 12 |
| 3 | 1000 | 8 |
| 4 | 500 | 8 |
| 5 | 1000 | 10 |
| 6 | 500 | 10 |
| 7 | 750 | 12 |
| 8 | 750 | 8 |
| 9 | 750 | 10 |

4.2.2.1. Determination of end-point of pelletization

Measurement of the impeller torque was used for the determination of pelletization end-point. It is a prevalent technique due to its reliability and in-process possibilities. The principle of this method is the detection of the resistance caused by the wet mass obstructing the impeller's movement. End-point was determined according to the profile of the impeller torque during production in the IV. phase of high-shear granulation (see Chapter 3.3.6.2.2.).

4.2.3. Manufacture of micropellets containing *nystatin* for application GIC therapy

Nystatin (Merck, Darmstadt, Germany), α -lactose-monohydrate (DC, BDI, Zwolle, Netherlands), microcrystalline cellulose (Avicel PH 105, FMC, Philadelphia, USA), hydroxyethylcellulose (HEC) (Hercules, Wilmington, USA) and carbomer (CPL) (Carbopol 934P, Hercules, Wilmington, USA) were used to prepare pellets. Purified water was used as granulation liquid. Quality of all materials used in the experiments was Ph. Eur. 7.

Pellets were produced in a high-shear mixer (Pro-C-epT 4M8 Granulator, Belgium, Zelzate) with a three-blade impeller and a chopper. Each batch contained 5% *nystatin*, 45% microcrystalline cellulose, hydroxyethylcellulose and carbomer in different amounts (0-5%) according to an experimental design, α -lactose-monohydrate added as diluent so that the total dry mass was 100.0 g. Powders were loaded into a 1000 ml bowl and premixed for 3 minutes. Purified water was used as binder liquid.

Pellets of 15 samples were prepared according to a central composite factorial design (Table IV. and V.) in triplicate. Experimental design of full type with five centre points had three numeric factors including average pellet size (x_1), CPL (x_2) and HEC (x_3) content and five coded levels (-1.414, -1, 0, +1, +1.414). Different average pellet sizes with various CPL and HEC contents were produced in the trials in order to examine different preparations. During statistical evaluations Design Expert v.7.0 (Stat-Ease Inc., Minneapolis, USA) was used to calculate the relative effect of factors (b), the confidence interval was 95%, significance was determined if $p < 0.05$. TableCurve® 3D v. 4.0 (Systat Software Inc., London, UK) was used to reveal the response surface from the polynomial equation calculated using the experimental design.

An Erweka vibrating sieve (Erweka GmbH, Heusenstamm, Germany) had been used for determining pellet size and separation of pellets by average size, according to the experimental design.

Table IV. Central composite factorial design with two level factorial design points (-1,1), axial points (-1.414, 1.414) and a centre point (0)

| Trial | x_1 | x_2 | x_3 |
|--------------|--------|--------|--------|
| 1 | 1 | 1 | -1 |
| 2 | 1 | -1 | 1 |
| 3 | -1 | 1 | 1 |
| 4 | -1 | -1 | -1 |
| 5 | -1.414 | 0 | 0 |
| 6 | 1.414 | 0 | 0 |
| 7 | 0 | -1.414 | 0 |
| 8 | 0 | 1.414 | 0 |
| 9 | 0 | 0 | -1.414 |
| 10 | 0 | 0 | 1.414 |
| 11 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 |

Table V. Process parameters of trials

| Factors with coded levels | -1.414 | -1 | 0 | 1 | 1.414 |
|---|---------------|-----------|----------|----------|--------------|
| x_1 , average pellet size (μm) | 217.2 | 300.00 | 500.00 | 700.00 | 782.8 |
| x_2 , CPL content (g) | 0.00 | 0.73 | 2.50 | 4.27 | 5.00 |
| x_3 , HEC content (g) | 0.00 | 0.73 | 2.50 | 4.27 | 5.00 |

4.2.4. Examinations of pellets

4.2.4.1. Particle size analysis

The size analysis of the pellets was carried out by sieves using an Erweka vibrating apparatus, with a set of eight standard sieves (100, 160, 250, 400, 630, 1000, 1600 μm). The sample size was 100.0 g and the shaking time was 5 minutes. The pellet size (geometric-weight mean diameter) and size distribution (geometric standard deviation) were estimated.

In case of optimized production *Rosin-Rammer-Sperling-Bennett* (RRSB) distribution function of particle size was also presented, based on the mass retained on the sieves, which is described by the following formula [21,73]:

$$R\% = 100 \cdot e^{-\left(\frac{x}{a}\right)^n} \quad (14)$$

where

| | |
|-------|-------------------------------------|
| $R\%$ | residual mass on the sieve |
| x | particle size |
| a | size at 36,8% of particles retained |
| n | uniformity factor |

Software for RRSB distribution was developed by our institute.

4.2.4.2. Drug release

Drug release from pellets containing *nystatin* was studied in 900 ml of pH 1.2 hydrochloric acid at $37 \pm 0.5^\circ\text{C}$, applying a paddle apparatus of Ph. Eur. 5. at 75 rpm (Erweka DT 700, Heusenstamm, Germany) examining 500 mg samples. Spectrophotometric determination was carried out according to previous examinations ($\lambda = 306 \text{ nm}$, Jasco V-550 UV/VIS spectrophotometer, Japan). Mean and standard deviation (S.D.) was determined from three samples.

The dissolution kinetics of the preparation detected by both spectrophotometer and microbiological method, was determined by the *Weibull* distribution function, applied in the following form [1]:

$$m_t = m_\infty \left(1 - e^{-\left[\frac{(t-t_0)}{\tau}\right]^\beta} \right) \quad (15)$$

where

| | |
|------------|--|
| m | dissolution (%) at time t |
| m_∞ | dissolution (%) at infinite time |
| t_0 | lag-time of dissolution |
| τ | mean dissolution time (theoretical time when 63.2% of the active agent is dissolved) |
| β | shape parameter of the dissolution profile |

Our evaluation focused mainly on the effect of matrix forming agents on drug release kinetics. Shape parameter β and mean dissolution time τ were selected to characterize drug release and the correlation was determined between the values of the microbiological assay and the spectrophotometric measurement. Regarding these parameters, β_S and τ_S were determined from spectrophotometric data, β_M and τ_M were determined from microbiological assay.

4.2.4.3. Determination of biological activity by direct bioautography

One of the most widely applied methods among biological activity measurements is the direct bioautography. In this method microorganisms grown in a proper broth are spread on the surface of a TLC plate and then incubated. The surface of the TLC plate is covered with the broth to ensure the growth of microorganisms. Antimicrobial agents dripped on the plate develop inhibition zones which can be easily visualised by application of dehydrogenase activity detecting substances [56].

Biological activity of the samples was determined on silica gel plates applying 3-(4, 5-dimethyl-2-thiazolyl)-2, 5-diphenyl-2H-tetrazolium bromide – MTT (Sigma Aldrich, USA) to visualise antimicrobial activity. The applied test strain was *Candida albicans*, ATCC 90028. The TLC plates were: TLC DC - Alufolien Silica gel 60 F254 (Art. 1.05554, Merck, Darmstadt, Germany). Sample application on TLC plates was a series of 2-7 ng *nystatin* (Fig. 16.). Samples of microbiological detection and UV spectrophotometric determination were from the dissolution experiment. The diameter of inhibition spots was determined by the analysis of brightness distribution on TLC plate using 300 dpi scanned images and *ImageJ 1.45f* software (Wayne Rasband, National Institutes of Health, USA) for evaluation.



Figure 16. Inhibition spots on a sample TLC plate

4.2.4.4. Bioadhesivity test

The bioadhesivity of the prepared micropellets was investigated *ex vivo* by a wash-off test. A 1.5x1.5 cm piece of guinea pig ileum mucosa was fixed onto a plate at an angle of 45°. The examined section of ileum was previously rinsed in a Krebs buffer solution of the following composition:

- NaCl (119 mmol/L)
- KCl (4.7 mmol/L)
- CaCl₂·2H₂O (2.5 mmol/L)
- NaHCO₃ (20 mmol/L)
- MgCl₂·7H₂O (1.17 mmol/L)
- KH₂PO₄ (1.18 mmol/L)
- EDTA (0.027 mmol/L)
- glucose (11 mmol/L)

Pellets ($n = \sim 50$) were gently spread onto the mucosa, then 50 ml of Krebs solution was applied to rinse at flow rate of 20ml/min. The number of pellets adhering to the tissue after rinsing were counted and compared to the total amount of the initial value in bioadhesion retention % [61].

4.2.4.5. Scanning electron microscopy examinations

Scanning electron microscope (JEOL, JSM 6300 Scanning Microscope, Japan) was used to study the surface and the shape of samples. For SEM evaluation the pellets were mounted on a worksheet and coated with fine gold. Acceleration voltage of 20.0 kV was used with 100x magnification.

4.2.4.6. Diffuse reflectance examinations

Diffuse reflectance measurement ($R\%$) was carried out on solid samples applying an UV/VIS/NIR spectrophotometer (Jasco V-670, Japan) equipped with integrating sphere (diameter=60mm) and PbS detector between 1000-2000 nm in a 5 mm layered cell. Reflectance was evaluated according to the *Kubelka-Munk* formula [62]:

$$F(R\%) = \frac{K}{S} = \frac{(1-R\%)^2}{2R\%} \quad (16)$$

where

$R\%$ intensity of diffusely reflected light

K absorption coefficient

S scattering coefficient

4.2.4.7. Swelling examinations

Swelling of pellets was determined using a calibrated stereomicroscope (Nikon SMZ 800 C-PS, Japan). During the examination $n = \sim 50$ pellets were suspended in 5 ml of distilled and degassed water. The increase in size of the pellets was monitored for 15 minutes and evaluated compared to the initial size [65].

4.2.4.8. Further dosage form examinations (bulk and tapped density, flowability, friability)

The bulk and tapped densities of the pellets were determined by standard methods. The tapped density was performed applying 1250 taps using a tapped density tester (J. Engelsmann, Ludwigshafen, Germany). The bulk and tapped density data were used to calculate the *Hausner's* [66] and *Carr's* [67] indices.

Flowability was examined using the apparatus described in the Ph. Eur. 7., 2.9.16. test, by application of a dry funnel calculating the angle of repose of 100.0 g sample preparation.

Friability examinations were carried out according to the Ph. Eur. 7. as well, using the apparatus in 2.9.7. test measuring 10.0 g of the sample. 100 rotations were made after the pellet's dust-control and then measured the loss of weight in % [68].

4.2.4.9. Stability test

Accelerated stability test of optimized product was carried out aiming the determination of the following parameters:

- k , degradation constant,
- $t_{1/2}$ half-life of the degradation and
- t_x expiration date.

Stability tests are based on the *Arrhenius* law:

$$k = A \cdot e^{-\frac{E_a}{RT}}, \quad (17)$$

At first order decomposition in case of *nystatin*, degradation half-life ($t_{1/2}$) can be calculated by the following way [74]:

$$t_{1/2} = \frac{0,693}{k} \quad (18)$$

The E_a activation energy can be determined by taking into account degradation constants at different test temperatures:

$$\log \frac{k_2}{k_1} = \frac{E_a}{2,303R} \left(\frac{T_2 - T_1}{T_2 \cdot T_1} \right) \quad (19)$$

According to the *Arrhenius* equation results of long term stability tests can be predicted by calculating the degradation constants at different temperatures (in my experiment it was 40, 50 and 60°C), then representing the $\log k-1/T$ function, by extrapolation the decay at 25°C can be calculated [35,75].

In case of expiration date 5% decay of the API was allowed, applying the formula:

$$t_x = \frac{2,303}{k} \log \frac{m_0}{m_0 - x} \quad (20)$$

Legends of the equations above:

| | |
|---------------|---|
| k, k_1, k_2 | degradation constants |
| A | pre-exponential factor (frequency factor) |
| E_a | activation energy |

| | |
|---------------|--------------------------------------|
| R | universal gas constant |
| T, T_1, T_2 | absolute temperature |
| $t_{1/2}$ | degradation half life |
| t_x | expiration date |
| m_0 | initial API content |
| x | decayed API amount during t_x time |

Simex Binder BF 115 thermostate was used to keep the samples on three different temperatures mentioned before at 75% relative humidity. Samples were taken monthly for 6 months. Total API content was determined by pulverizing the pellets and dissolving the API in 50 ml of methanol containing 5% acetic acid accelerating the dissolution by KL-2 Bühler shaking machine for 6 hours. After filtration *nystatin* content was determined ($\lambda = 306$ nm, Jasco V-550 UV/VIS spectrophotometer, Japan).

5. Results

5.1. Optimization results for high-shear pelletization

Considering the average particle size ($y_1, R = 0.981$), both process variables significantly influenced the particle agglomeration process through the model of the next formula:

$$y_1 = 1519.846 + 1.572x_1 - 266.98x_2 + 0.0558x_1x_2 - 0.0014x_1^2 + 9.829x_2^2 \quad (21)$$

The positive sign of the coefficients refers to an increasing effect while the negative sign indicates a decreasing effect on the corresponding response.

Increasing the binder flow rate the reduction of the average particle size was observed, which is probably due to the faster agglomeration, where more pellets were formed with smaller size within a shorter period. The impeller speed had opposite effect on particle size depending on its value. In the first stage (up to 750 rpm), the impeller helped the formation of larger particles, above 750 rpm, smaller particles were built due to intensive agitation which may hinder the further agglomeration of pellets (Fig. 17.).

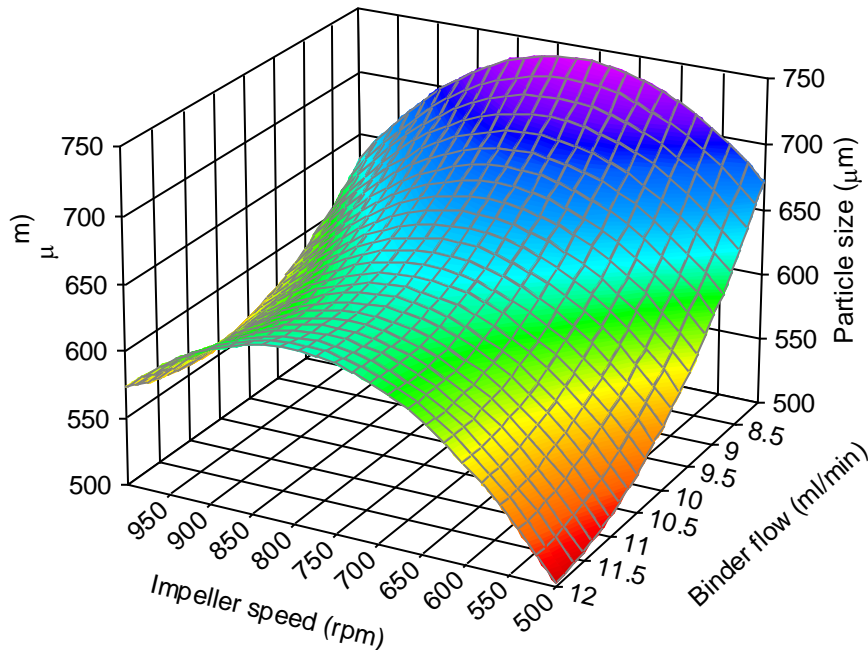


Figure 17. Effect of impeller speed and binder flow on the average particle size

Table VI. Measurements according to the experimental design

| Trial | Controlled factor | | |
|-------|-------------------------------------|-------------------------------------|--|
| | x_1 Impeller speed (rpm) | x_2 Binder flow (ml/min) | y_1 Particle diameter (μm) |
| 1 | 1000 | 12 | 583.8 ± 22.33 |
| 2 | 500 | 12 | 513.7 ± 26.67 |
| 3 | 1000 | 8 | 628.4 ± 33.42 |
| 4 | 500 | 8 | 669.8 ± 29.56 |
| 5 | 1000 | 10 | 596.4 ± 22.41 |
| 6 | 500 | 10 | 550.0 ± 15.67 |
| 7 | 750 | 12 | 628.4 ± 21.34 |
| 8 | 750 | 8 | 770.0 ± 39.12 |
| 9 | 750 | 10 | 632.7 ± 32.17 |

Table VII. Statistical evaluation of measurements

| Response | Model F - value | Parameter | Coefficients | | | | | |
|----------------------|----------------------|-----------|--------------|-------|----------|----------|--------------|--------------|
| | | | b_0 | b_1 | b_2 | b_{11} | b_{22} | b_{12} |
| Particle diameter | 15.20 | Value | 1519.846 | 1.572 | -266.979 | -0.0014 | 9.831 | 0.056 |
| | | Std error | 464.235 | 0.463 | 84.792 | 2.65E-04 | 4.141 | 0.023 |
| | | $p > t $ | 0.05 | 0.04 | 0.05 | 0.01 | 0.10 (NS) | 0.10 (NS) |

Diffuse reflectance spectra of pellet samples manufactured in the 9 experimental trials demonstrated significant differences depending on the impeller speed and binder flow rate (Fig. 18.). Pellet samples with large average particle diameter demonstrated an elevated spectral shift through $F(R)$ values, offering benefits for the in-process control, such as end-point determination of the pelletization process by NIRS. A linear regression was established between the particle size and transformed reflectance values according to the *Kubelka–Munk* formula ($R=0.9842$) (Fig. 19.).

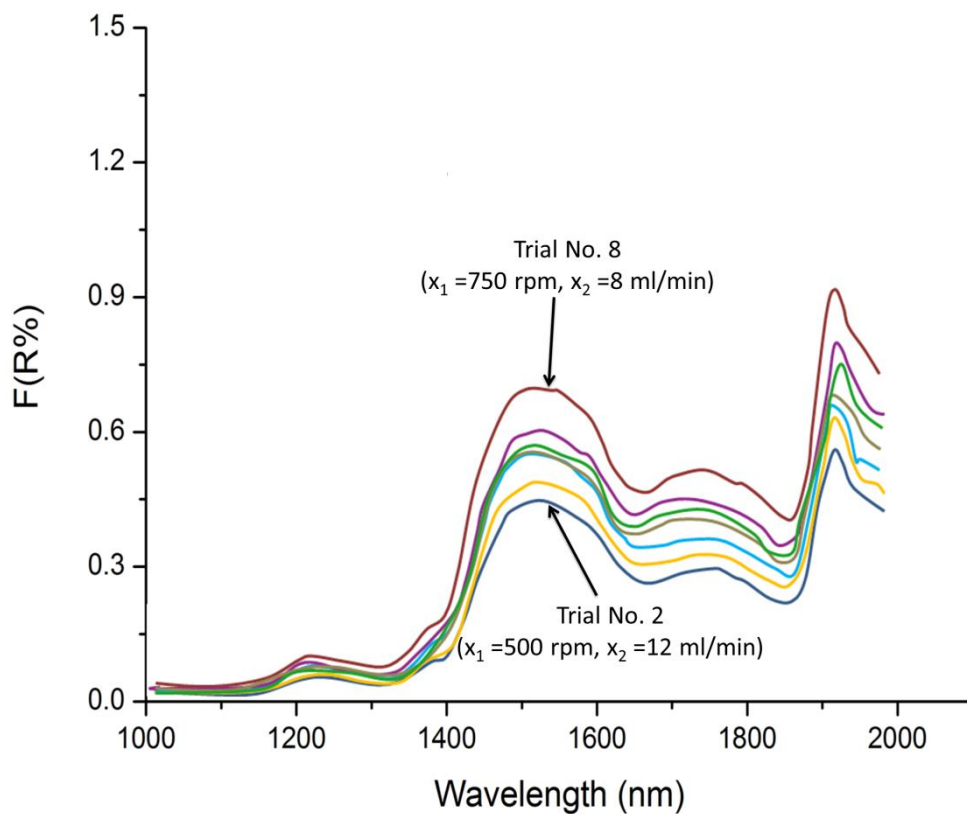


Figure 18. Diffuse reflectance spectra of samples according to *Kubelka-Munk* formula (see Chapter 4.2.4.6.)

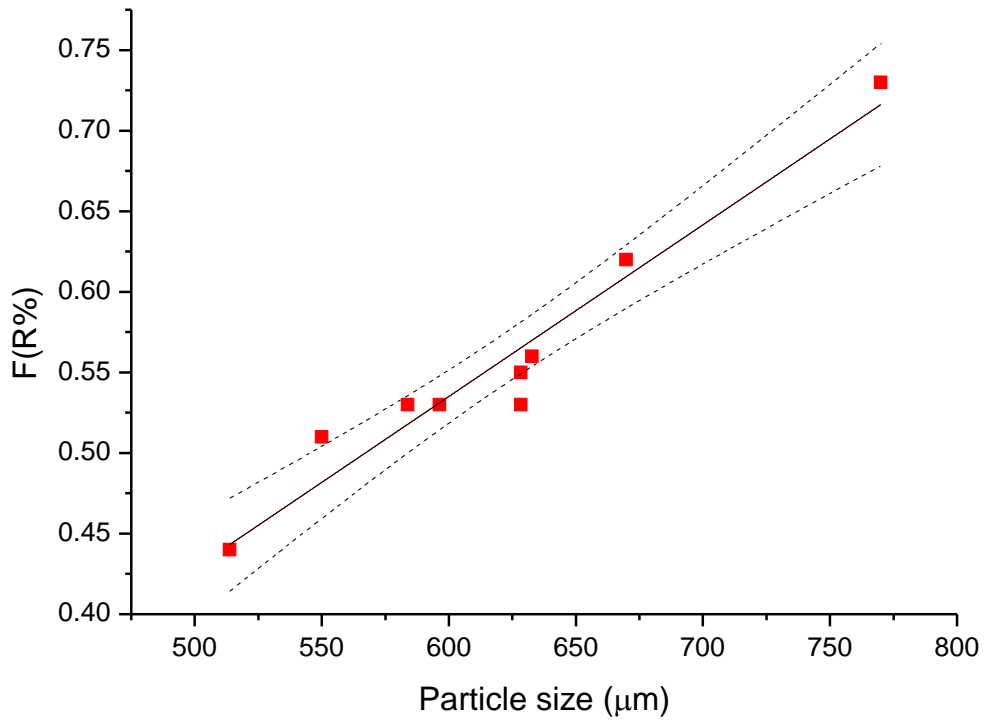


Figure 19. Correlation between the particle size of micropellets and diffuse reflectance spectra after *Kubelka-Munk* transformation at 1528 nm representing 95 % confidence interval

5.2. Results of examinations of nystatin micropellets

Results of our second manufacture based on preliminary examinations according the central composite experimental design (Table IV.) are described in Table VIII.

Table VIII. Matrix of the central composite experimental design (τ_S – mean dissolution time based on spectrophotometric data, τ_M – mean dissolution time based on microbiological assay, β_S – Weibull's shape parameter based on spectrophotometric data, β_M – Weibull's shape parameter based on microbiological assay)

| Tr. | Examined factors | | | Response parameters (Mean±S.D., $n=3$) | | | | Swelling (μm) | Bioadhesion retention (%) |
|-----|---|------------|------------|---|--------------|-----------------------|---------------|-------------------------------|---------------------------------|
| | x_1 | x_2 | x_3 | Spectrophotometric data | | Microbiological assay | | | |
| | Average particle size (μm) | CPL (%) | HEC (%) | τ_S (min) | β_S | τ_M (min) | β_M | | |
| 1 | 700.0 | 4.27 | 0.73 | 119.5±10.8 | 0.3519±0.011 | 103.2±5.2 | 0.3462±0.0432 | 58.2±0.80 | 57.44±1.02 |
| 2 | 700.0 | 0.73 | 4.27 | 56.9±7.3 | 0.5362±0.012 | 49.0±2.1 | 0.5103±0.014 | 10.4±1.12 | 43.63±2.04 |
| 3 | 300.0 | 4.27 | 4.27 | 283.2±21.4 | 0.4023±0.042 | 278.0±13.6 | 0.3789±0.023 | 18.0±1.76 | 42.24±1.67 |
| 4 | 300.0 | 0.73 | 0.73 | 16.7±0.7 | 0.3134±0.010 | 11.3±1.1 | 0.2970±0.064 | 6.8±0.82 | 12.65±2.32 |
| 5 | 217.2 | 2.50 | 2.50 | 4.1±0.9 | 0.3898±0.047 | 3.6±0.4 | 0.3567±0.010 | 1.3±1.20 | 36.31±0.78 |
| 6 | 782.8 | 2.50 | 2.50 | 287.3±40.1 | 0.5131±0.028 | 227.3±2.4 | 0.5108±0.022 | 41.4±0.33 | 68.52±2.21 |
| 7 | 500.0 | 0.00 | 2.50 | 16.3±6.5 | 0.5044±0.035 | 11.9±1.2 | 0.4890±0.035 | 4.6±1.43 | 33.21±2.42 |
| 8 | 500.0 | 5.00 | 2.50 | 87.3±15.6 | 0.3918±0.057 | 71.8±8.6 | 0.3675±0.014 | 43.4±0.65 | 47.78±2.10 |
| 9 | 500.0 | 2.50 | 0.00 | 43.4±13.2 | 0.4251±0.030 | 42.4±10.9 | 0.4172±0.023 | 13.7±1.66 | 49.50±1.10 |
| 10 | 500.0 | 2.50 | 5.00 | 82.1±17.8 | 0.4978±0.038 | 51.8±7.4 | 0.4356±0.014 | 16.9±0.37 | 31.85±0.43 |
| 11 | 500.0 | 2.50 | 2.50 | 404.3±58.4 | 0.4112±0.013 | 316.8±21.4 | 0.3983±0.030 | 32.1±0.45 | 38.42±0.80 |
| 12 | 500.0 | 2.50 | 2.50 | 329.4±11.1 | 0.4212±0.027 | 320.7±24.2 | 0.4171±0.022 | 36.0±0.98 | 37.43±1.64 |
| 13 | 500.0 | 2.50 | 2.50 | 332.3±6.7 | 0.4154±0.057 | 249.1±31.1 | 0.4056±0.020 | 38.3±0.41 | 32.64±1.30 |
| 14 | 500.0 | 2.50 | 2.50 | 333.1±15.7 | 0.4190±0.021 | 313.4±18.6 | 0.3989±0.013 | 40.4±0.65 | 35.81±0.93 |
| 15 | 500.0 | 2.50 | 2.50 | 274.2±54.2 | 0.4287±0.049 | 269.5±13.3 | 0.3752±0.025 | 40.6±0.48 | 31.93±0.64 |

Our evaluation focused mainly on the effect of matrix forming agents on drug release kinetics and bioadhesion. Shape parameter β and mean dissolution time τ were selected to characterize drug release and the correlation was determined between the values of the microbiological assay and the spectrophotometric measurement. β_S and τ_S were determined from spectrophotometric data, β_M and τ_M were determined from microbiological assay.

Results of UV dissolution and microbiologically detected studies are summarized in Table VIII. The inhibition spot images of trial No. 4, evaluated by software *ImageJ 1.45f* are shown in Fig. 20.



Figure 20. Microbiologically Detected Dissolution (MDD) series of trial No. 4

Investigating the relationship between the spectrophotometric and microbiological detection, linear correlation can be observed both in mean dissolution time ($R=0.9836$) (Fig. 21.) and in the *Weibull's* shape parameter ($R=0.9593$) (Fig. 22.). However, performing a paired two-sample t-test, there is a significant difference between the means in both cases ($p<0.05$). This phenomenon is supposed to be due to the higher sensitivity of the microbiological assay. To confirm the sensitivity of the methods, the minimal limit of detection of *nystatin* was determined both using the microbiological and the spectrophotometric method. According to the linear range of calibration points the microbiological activity of *nystatin* was detected in concentration $0.8 \text{ ng}/\mu\text{l}$ on TLC plate applying digital image analysis of inhibition spots, while limit of detection of spectrophotometric determination was $2 \text{ ng}/\mu\text{l}$. In both cases the applied solvent was pH 1.2 hydrochloric acid.

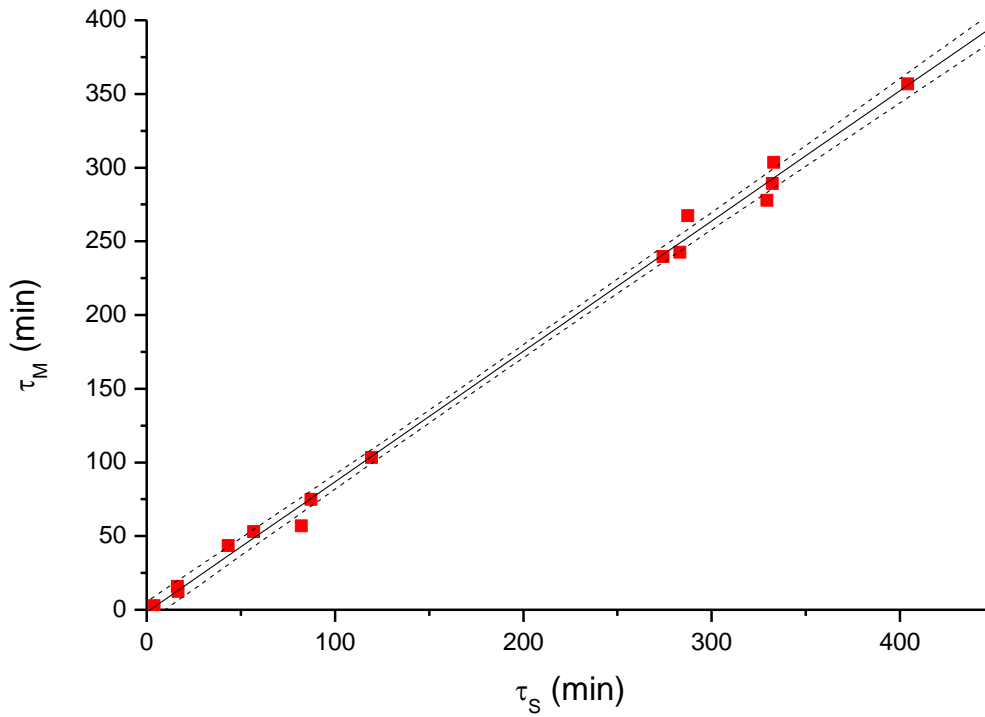


Figure 21. Correlation between the mean dissolution times calculated from the spectrophotometric and microbiological data (representing 95% upper and lower confidence intervals)

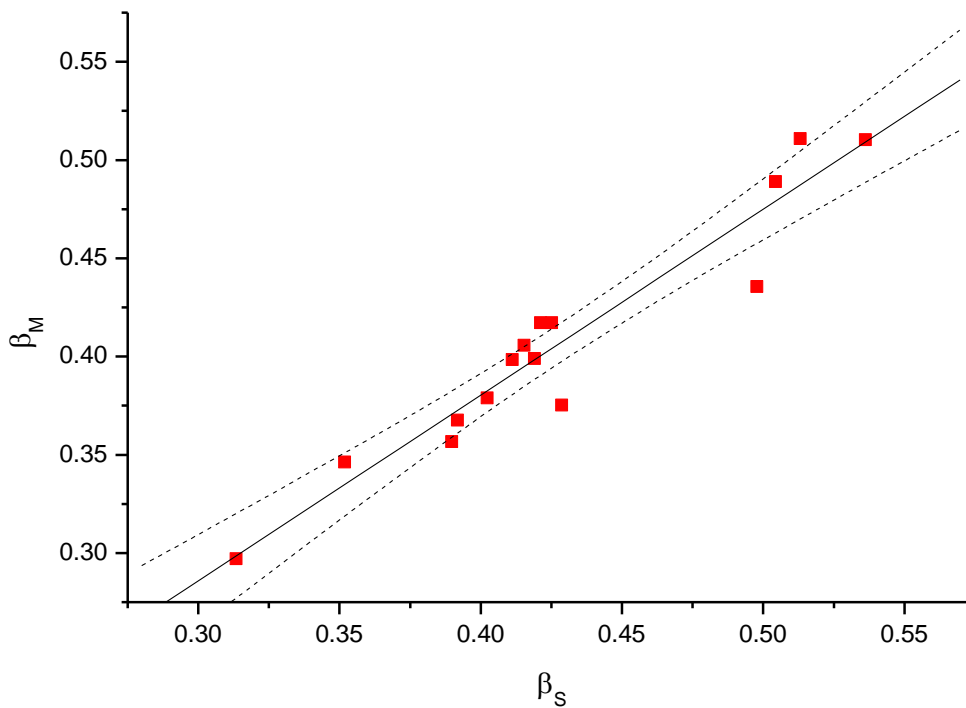


Figure 22. Correlation between the shape factors of the *Weibull* function calculated from spectrophotometric and microbiological data (representing 95% upper and lower confidence intervals)

Evaluating the dissolution curves, significant difference can be observed, since the presence of CPL and HEC slowed drug release remarkably, which is undesirable in this preparation. Fig. 23. presents the dissolution curves of trials 7, 9 and 12 as detected by both microbiological and spectrophotometrical method. The complete absence of CPL or HEC resulted in enhanced dissolution in trials no. 7 and 9.

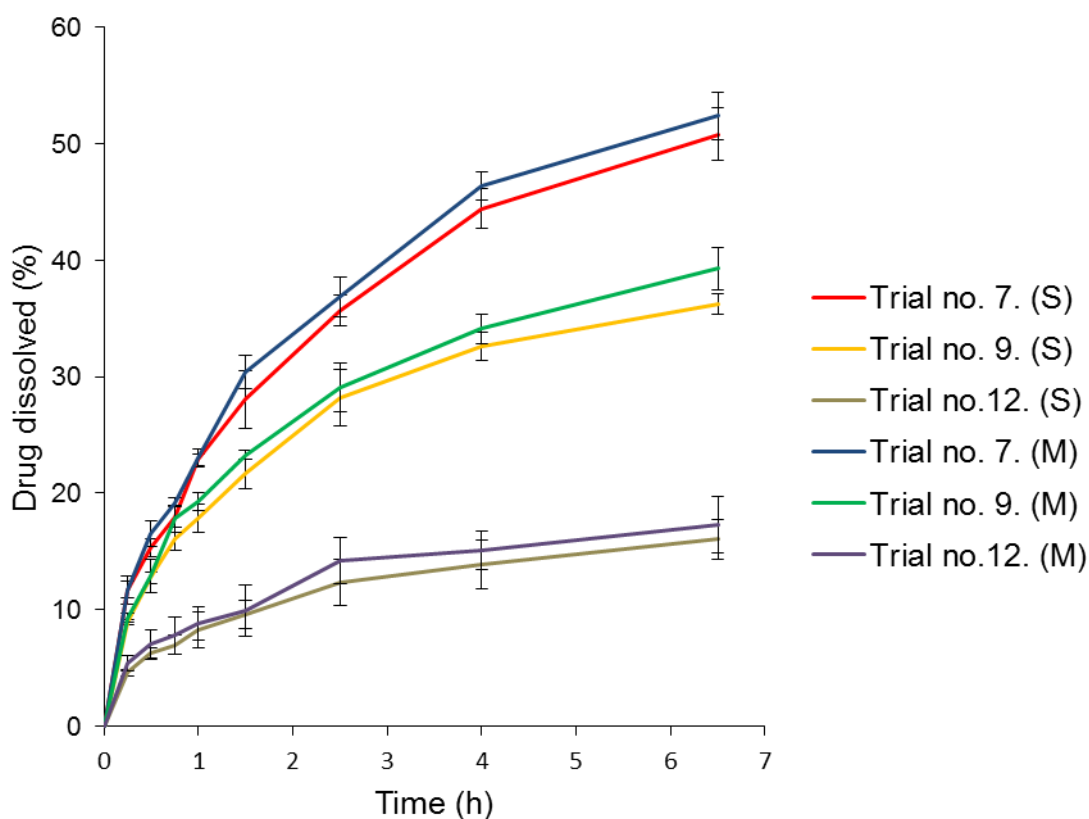


Figure 23. Dissolution of trials 7, 9. and 12 detected by both by spectrophotometric and microbiological method (S – spectrophotometric assay, M – microbiological assay)

Comparing and considering the measurements of the microbiological and spectrophotometric detection, the more sensitive microbiological tests were evaluated in further investigations. The equations of response surfaces represent the significant effects of factors x_1 and x_2 on the τ_M time parameter ($R=0.9908$), the β_M shape factor ($R=0.8535$), the bioadhesion retention time ($R=0.8262$) and the swelling ($R=0.8415$).

Table IX. represents the multiple regression statistical evaluation for significance and probabilities at 95% confidence interval of responses (*NS* = not significant).

Table IX. Statistical evaluation of the central composite factorial design

| Response | Model F -value | Parameter | Coefficients | | | | | | | | | | |
|-------------|--------------------|-----------|--------------|--------|----------------|----------------|----------------|----------------|----------|---------|---------|---------|-----------|
| | | | b_0 | b_1 | b_2 | b_3 | b_{12} | b_{13} | b_{23} | b_1^2 | b_2^2 | b_3^2 | b_{123} |
| τ_M | 21.32 | Value | 293.91 | 79.10 | 21.20 | 3.32 | -49.79 | -59.03 | 113.36 | -89.24 | -126.02 | -123.41 | -155.16 |
| | (p=0.0048) | Std error | 19.08 | 21.34 | 21.34 | 21.34 | 30.17 | 30.17 | 30.17 | 17.85 | 17.85 | 17.85 | 35.06 |
| | | p> t | - | 0.0082 | 0.2619 (NS) | 0.8480 (NS) | 0.0961 (NS) | 0.0620 (NS) | 0.0078 | 0.0028 | 0.0008 | 0.0008 | 0.0044 |
| β | 9.84 | Value | 0.410 | 0.050 | -0.032 | 0.034 | - | - | - | - | - | - | - |
| | (p=0.0019) | Std error | 9.16E-003 | 0.013 | 0.013 | 0.013 | - | - | - | - | - | - | - |
| | | p> t | - | 0.0022 | 0.0279 | 0.0203 | - | - | - | - | - | - | - |
| Swelling | 8.89 (p=0.0028) | Value | 26.81 | 12.56 | 14.23 | -4.01 | - | - | - | - | - | - | - |
| | | Std error | 2.74 | 3.76 | 3.76 | 3.76 | - | - | - | - | - | - | - |
| | | p> t | - | 0.0065 | 0.0030 | 0.3087 (NS) | - | - | - | - | - | - | - |
| Bioadhesion | 7.89 (p=0.0044) | Value | 11.15 | 0.038 | 4.526 | -0.649 | - | - | - | - | - | - | - |
| | | Std error | 2.11 | 2.88 | 2.88 | 2.88 | - | - | - | - | - | - | - |
| | | p> t | - | 0.0022 | 0.0181 | 0.6983 (NS) | - | - | - | - | - | - | - |

According to the modified cubic response surface the average size of the pellets, its quadratic form, the quadratic form of CPL and HEC and the interaction between the CPL and the HEC influence the effect of *nystatin* significantly. Smaller size of the pellets results better dissolution due to the large specific surface. Pellets with average size from 500 to 1000 μm containing CPL and HEC in app, in ratio 1:1, have the slowest drug release profile (Fig. 24. and Fig. 25.). In this case the area of the maximum point is not recommended as aim during production.

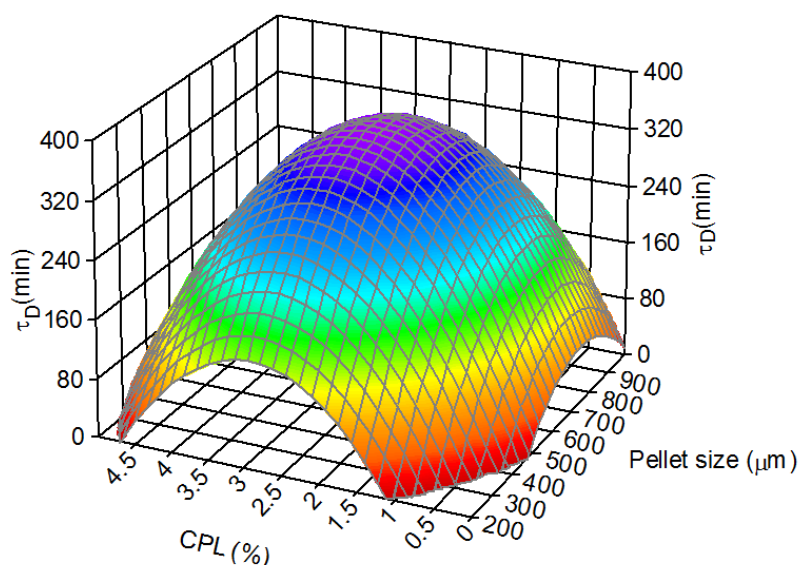


Figure 24. Effect of pellet size and CPL content on Mean Dissolution Time (2.5% HEC content)

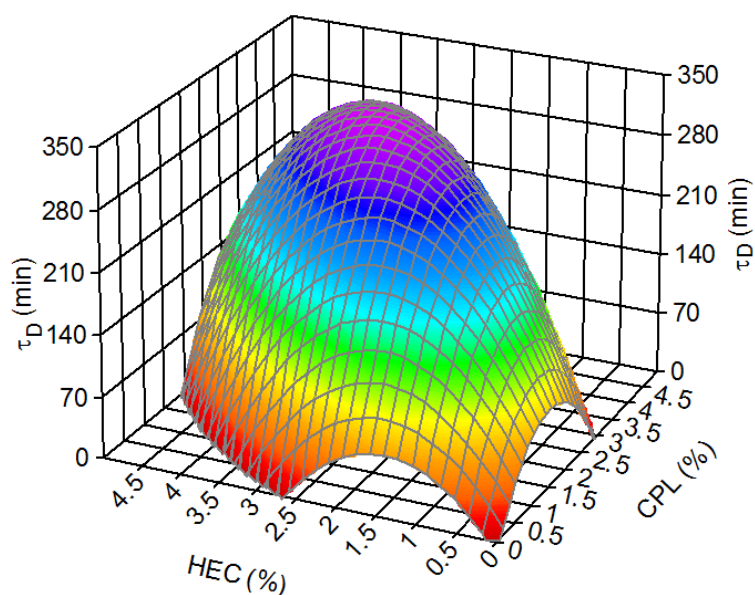


Figure 25. Effect of CPL and HEC content on Mean Dissolution Time (500 μm pellet size)

The *Weibull* function's shape parameter β is influenced significantly by pellet size, CPL and HEC content. The relationship is described with a linear model. The shape parameter increases with the increase of pellet size. Simultaneous increase of HEC and decrease of CPL results in a higher β value (Fig. 26. and Fig. 27.).

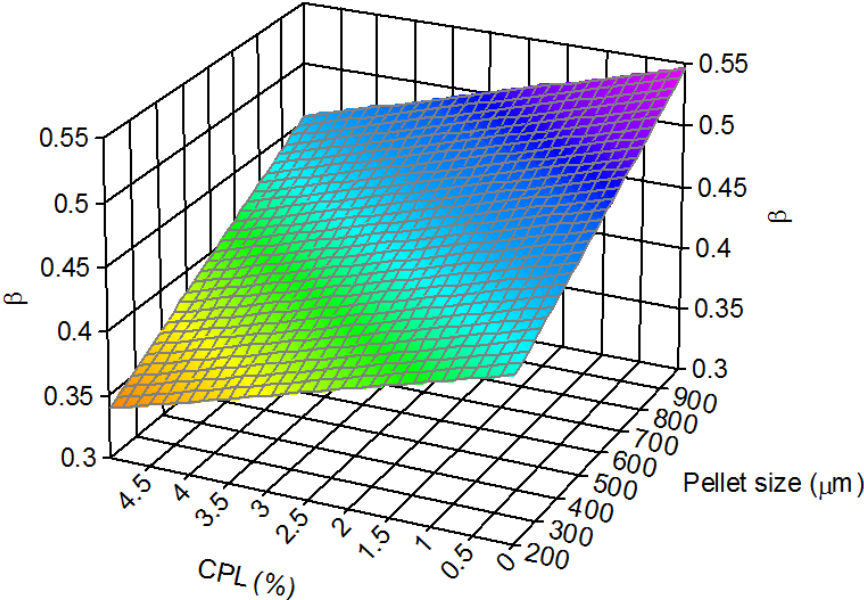


Figure 26. Effect of pellet size and CPL content on the *Weibull's* β_M shape parameter (2.5% HEC content)

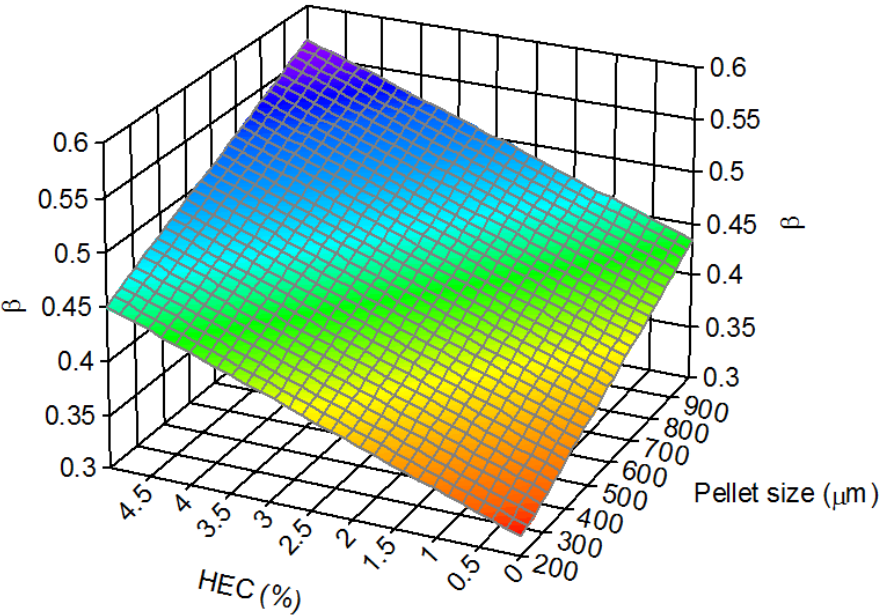


Figure 27. Effect of pellet size and HEC content on the *Weibull's* β_M shape parameter (2.5% CPL content)

Linear effect can be observed on Fig. 28. representing the swelling character of the samples. HEC has no significant effect, but increasing amount of CPL significantly increases the swelling ability.

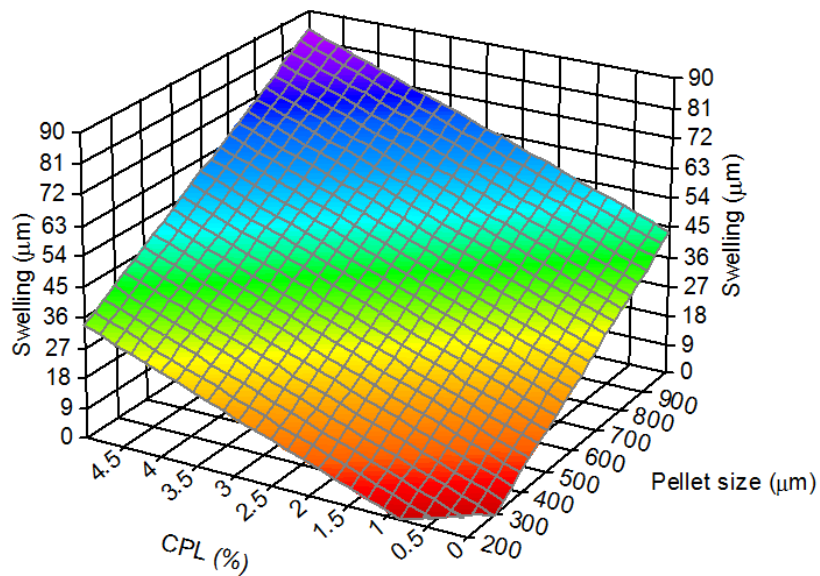


Figure 28. Effect of pellet size and CPL content on the swelling properties of pellets (2.5 % HEC content)

There are two significant factors (x_1 and x_2) concerning the linear model of bioadhesive retention. Contemporaneous increase in pellet size and CPL content produces higher bioadhesion rates (Fig. 29.). HEC content has no significant effect in this model.

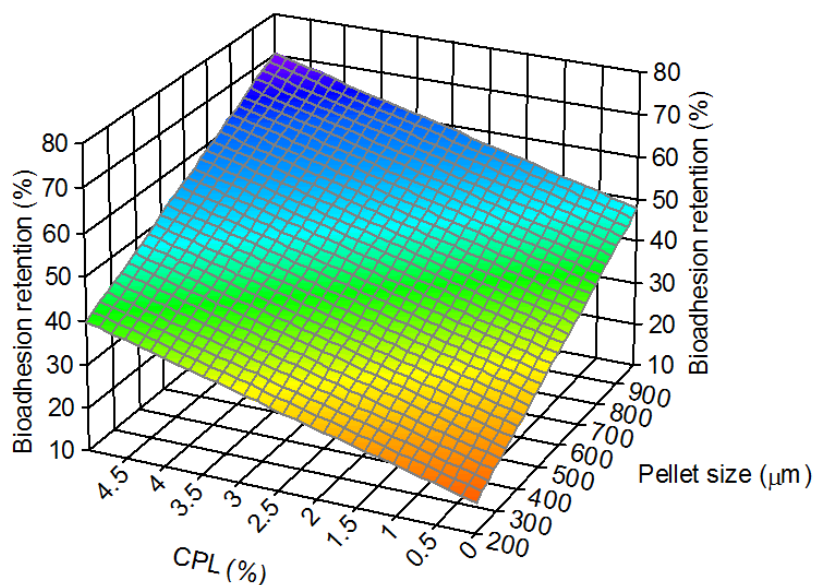


Figure 29. Effect of pellet size and CPL content on the ex vivo bioadhesion of pellets (2.5 % HEC content)

Trials 7, 9 and 12 were selected from the samples to be investigated by scanning electron microscopy with the same pellet size (500 μ m), but different ratios of CPL/HEC:

- Trial No. 7, CPL 0%, 5% HEC
- Trial No. 9, 5% CPL, 0% HEC
- Trial No. 12, 2.5% CPL, 2.5% HEC

The manufacturing process parameters were the same in all trials, thus the character of the surface of the pellets depends only on the CPL/HEC ratio. In trials No. 7, and 9 where either carbomer or hydroxyethylcellulose was used as bioadhesive agent, the surfaces of pellets were almost similarly porous. Samples from trial No. 12 containing CPL/HEC in ratio 1:1 were fine and glossy. This smooth surface is due to the congealment of the applied bioadhesive polymers which results slow release of the API (Fig. 30.).

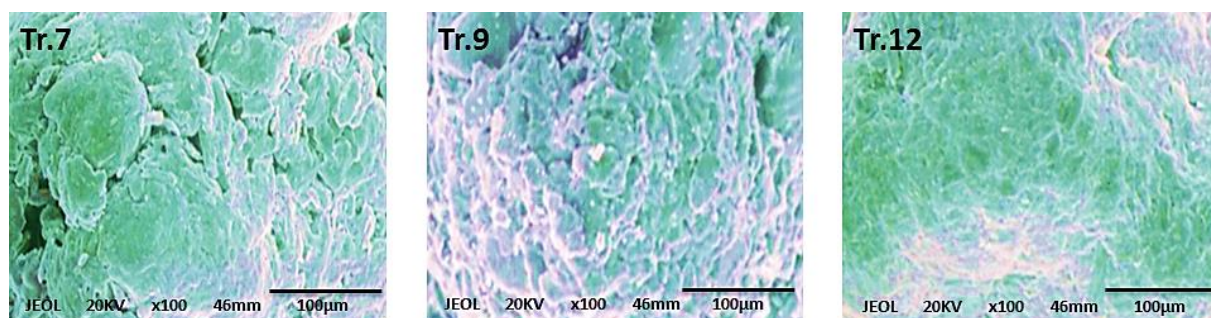


Figure 30. SEM image of micropellets from trials No. 7., 9., 12.

The diffuse reflectance spectra of pellet samples from trials No. 7, 9 and 12 with the same particle size of 500 μ m were also analysed as a function of CPL and HEC content, which may refer to the surface characteristics of the samples [70]. Significant difference can be observed in trial No. 12, with elevated spectral shift caused by the glossy surface characteristics (Fig. 31.).

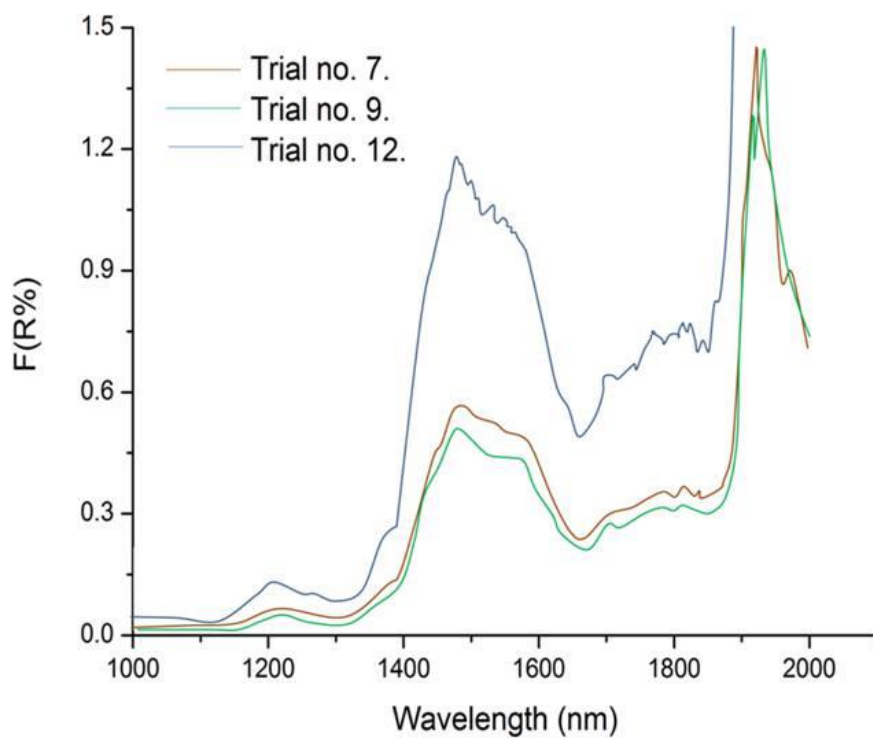


Figure 31. Diffuse reflectance spectra of pellet samples (Trials No. 7, 9 and 12) after *Kubelka-Munk* transformation (see Chapter 4.2.4.6.)

6. Discussion

The aim of the dissertation was to develop an optimized drug delivery system in order to treat gastrointestinal candidiasis. The fundamental point of an effective therapy may be a locally acting antifungal agent incorporated in a multiparticulate dosage form. As the active pharmaceutical ingredient, *nystatin* was chosen due to its advantageous properties of having contact antimicrobial effect with negligible absorption. As the dosage form micropellets were produced due to their good physical properties and large contact surface uniformly spreading through the GI tract. For production method among several possibilities high-shear pelletization was chosen, which is a reliable and quick method offering numerous facilities via adjustment of process parameters affecting the properties of the end-product. Optimized GIC therapy also requires long retention time on the surface of action which can be ensured by application of bioadhesive excipients, such as CPL and HEC. Summarizing the facts and observations, by production of *nystatin* based micropellets containing bioadhesive materials optimized GIC therapy can be reached.

In order to achieve the aims, preliminary examinations were carried out on a high-shear granulator to determine significant process parameters affecting the physical properties of micropellets focusing on the particle size distribution. These examinations were made according to a 3-level face-centred central composite experimental design examining the effect of impeller speed and binder flow rate on micropellet parameters.

After evaluation of the experiments a second order polynomial model was set up, which pointed to both factors as significant process parameters representing their effect as a saddle shape function. This experiment represented, that by applying extremities of the impeller speed (500 rpm and 1000 rpm) and liquid addition at speed of 10-12 ml/min together resulted relatively small particle size (500-550 μm). End-point of pelletization was determined by the measurement of the impeller torque. According to the experiments detection of NIR spectra after appropriate transformation could also serve important information of the process, since close ($R=0.9842$) correlation was observed between the particle size and the diffuse reflectance of the samples.

Results of these preliminary examinations were applied in the preparation of *nystatin* containing micropellets, adjusting process variables according to the previous experiences.

In the second production experimental design of full type with five centre points was set up. Examined factors were the following:

- average pellet size,
- CPL content and
- HEC content.

Investigated quality parameters of micropellets were:

- particle size distribution,
- flowability,
- hardness,
- surface characteristics,
- swelling,
- bioadhesion property and
- dissolution of nystatin determined by spectrophotometer and microbiological assay.

Evaluating the results important observation was the applicability of microbiologically detected dissolution based on direct bioautography, which had close correlation with the drug release determined by spectrophotometric method regarding both the mean dissolution time (MDT) and the shape factor (β) of the *Weibull* distribution applied as a model for the dissolution studies. Extremities of the micropellet size (~200 μm and ~800 μm), CPL and HEC content (at both excipients 0 and 5%) short dissolution time could be achieved. According to the model established low value of shape factor, which was also the aim of the optimization, could be reached by reducing the pellet size and HEC content, but increasing CPL content. In case of swelling, particle size and CPL content was significant. Increasing CPL content and particle size swelling ratio also increased. Surface characteristics by SEM clearly represented the matrix formation of CPL and HEC when applied in the same amount, which was also confirmed by the diffuse reflectance spectra, since in this experiment it was not the indicator of the particle size, but the surface roughness of micropellets.

6.1. Optimization of GIC therapy

Gathering all experimental data and determining the optimization aims (short dissolution time and low β values with long retention time with appropriate swelling) software Design Expert v.7.0 (Stat-Ease Inc., Minneapolis, USA) was used to calculate the recommended parameters for the optimized GIC therapy by micropellet based drug delivery system.

Result of the optimization is production of *nystatin* containing micropellets with average size of 550 μ m, containing about 4.25% CPL and 0.75% HEC. To confirm the optimization result, a test sample was produced in triplicate.

Pellets production was carried out according to the previous experiences in a high-shear mixer (Pro-C-epT 4M8 Granulator, Belgium, Zelzate) with a three-blade impeller and a chopper. Powders were loaded into a 1000 ml bowl and premixed for 3 minutes. Ingredients and excipients were 5% *nystatin* (Merck, Darmstadt, Germany), 45% α -lactose-monohydrate (DC, BDI, Zwolle, Netherlands), 45% microcrystalline cellulose (Avicel PH 105, FMC, Philadelphia, USA), 0.75% hydroxyethylcellulose (Hercules, Wilmington, USA) and 4.25% carbomer (Carbopol 934P, Hercules, Wilmington, USA). Quality of all materials used in the experiments was Ph. Eur. 7. The total dry mass was 100.0 g. 50 ml of purified water was used as granulation liquid at speed of 10 ml/min. Production was carried out at 25°C with 5 min net pelletization time applying 500 rpm impeller and 2000 rpm chopper speed.

Pelletization end-point (Fig. 32.) was determined according to the impeller torque in pelletization phase IV (see Chapter 3.3.6.2.2).

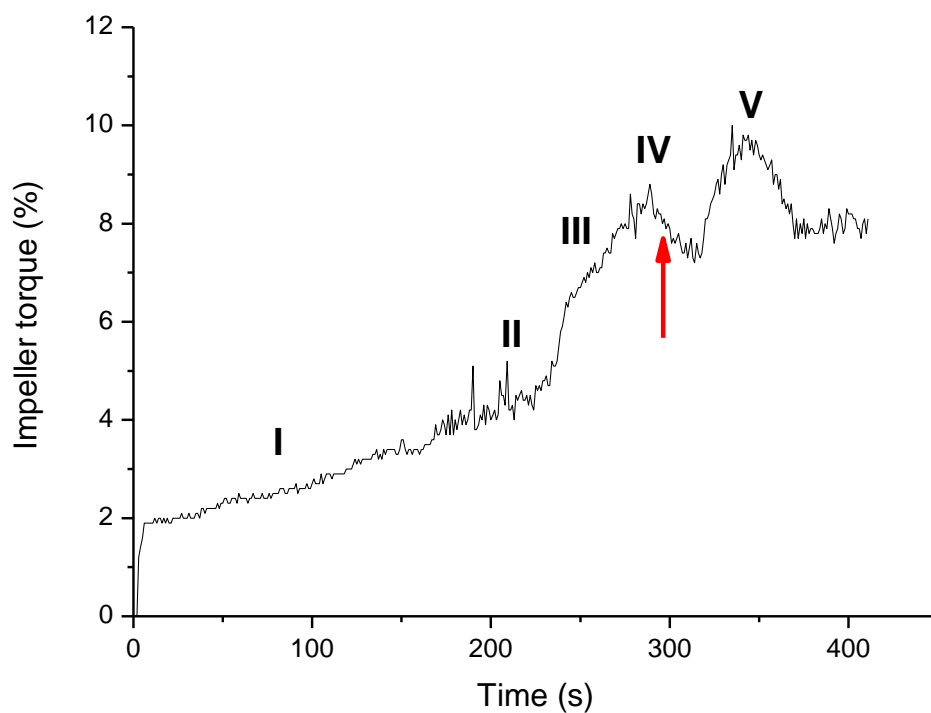


Figure 32. Pelletization end-point in case of optimized production (end-point marked with red arrow)

Examinations carried out were the following: average particle size, mean dissolution time, *Weibull* shape factor, flowability, Carr index, Hausner factor and friability.

Before examinations pellets were kept in a closed container for 24 h. Examination of these pellets were carried out in triplicate to test the optimization results (Table X.).

Table X. Results of examinations of optimized micropellets

| Property | Result | Desired value |
|-------------------------------|-------------------------|---------------|
| Average particle size | 564.7±23.3 μm | 550 μm |
| τ_D | 5.7±2.1 | 5-10 min |
| β | 0.3872±0.032 | 0.3-0.5 |
| Bioadhesion retention | 55.3±2.7 % | 50-55% |
| Swelling | 50.7±4.2 μm (8.8%±0.7%) | >5% |
| Flowability (angle of repose) | 24.40°±3.18° | <25° |
| Carr index | 10.71±0,23 | <10 |
| Hausner factor | 1.12±0.05 | <1.25 |
| Friability | < 0.5% | <1% |

Fig. 33. represents the RRSB particle size distribution function of the optimized micropellets with the following linearized relationship (R=0.9779):

$$y = -4.378 \cdot x + 11.169 \quad (22)$$

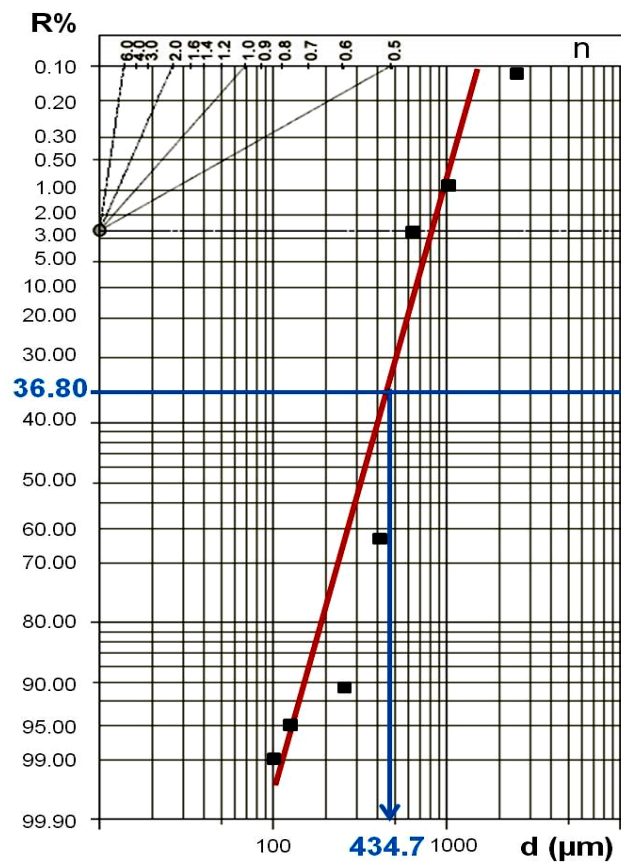


Figure 33. RRSB particle size distribution function of optimized micropellets

The particle size distribution of the optimized micropellets is monodisperse. According to the RRSB diagram the characteristic particle size parameter (d) at 36.8% is $434.7 \pm 15.3 \mu\text{m}$ and the uniformity factor: $n = 4.378$.

The dissolution curve of these samples is in Fig. 34. Results from stability tests are presented in Table XI. and Fig. 35.

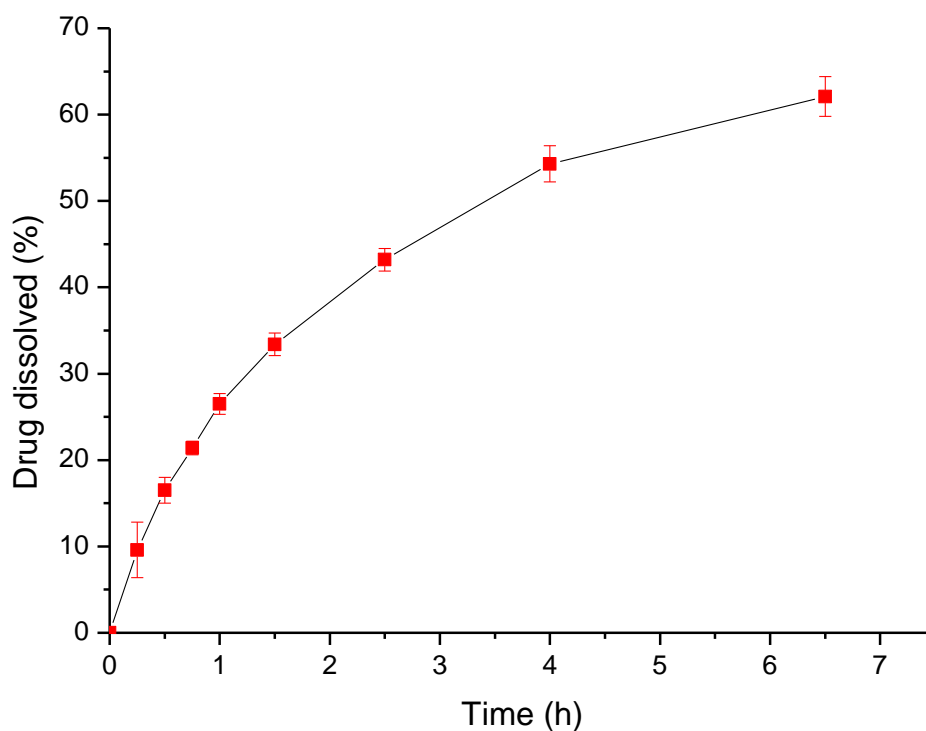


Figure 34. Dissolution curve of the optimized micropellets

Table XI. Results of stability tests

| Temperature ($^{\circ}\text{C}$) | <i>Nystatin</i> degradation | |
|------------------------------------|-----------------------------|-----------------------------|
| | $t_{1/2}$ (months) | k (month^{-1}) |
| 25 | 320.2 | 0.0022 |
| 40 | 76.4 | 0.0091 |
| 50 | 34.1 | 0.0203 |
| 60 | 2.3 | 0.3013 |

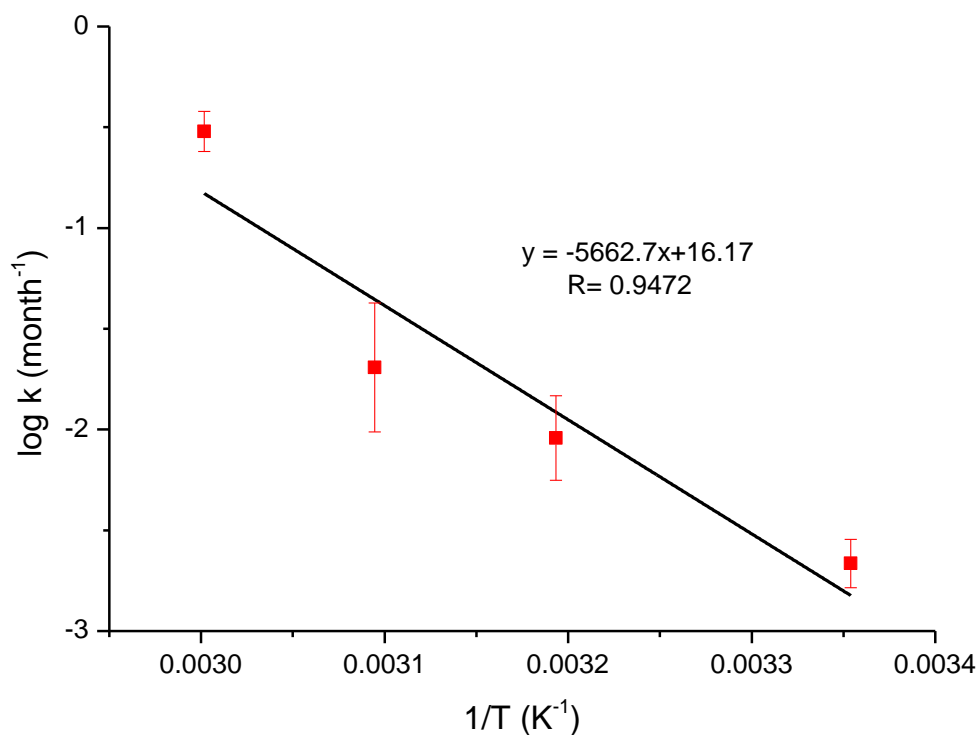


Figure 35. Stability test of the optimized sample

According to the Arrhenius law and my measurements, allowing 5% decay of the *nystatin*, expiration date: $t_x = 34.18$ months.

As it can be seen a thorough examination was carried out containing further tests according to the Ph. Eur. 7. beside the tests closely connected to the optimization results. According to the guidelines of Ph. Eur. 7. and scientific literature [67] the test production fulfilled all the criteria specified before thus facilitating an optimized GIC therapy.

6.2. Summary of the new results

According to my preliminary and optimizational examinations new results of my research work are the following:

1. In my experiments impeller speed and binder flow rate were found as significant process parameters influencing the pellet size during high-shear pelletization.

2. It can be declared, that impeller torque and diffuse reflectance measurement can both be used in in-process control of high-shear pelletization including the determination of the end-point of the manufacturing process.
3. Measurement of diffuse reflectance was found to be an indicator of the surface characteristics of micropellets which was confirmed by SEM examinations.
4. According to the results application of Microbiologically Detected Dissolution (MDD) studies based on direct bioautography were able to modelize the antifungal effect of the *nystatin*.
5. Close correlation was found between spectrophotometric investigations and MDD studies.
6. Experiments verified that by incorporating bioadhesive materials, such as CPL and HEC in the pellet matrix, the residence time significantly increases on the surface of the mucous membranes.
7. According to the optimizational results of my research work optimal ratio of CPL:HEC was determined to be 17:3 to reach 50-55% bioadhesion retention and relatively quick dissolution (MDT=5-10min).
8. Optimal size of pellets in my experiments aiming GIC therapy is found to be 550 μ m.
9. Summarizing my results recommendation for the ingredients and their proportions in an optimized GIC therapy by production of micropellets with 550 μ m average particle size may be:
 - *nystatin* (5%)
 - *microcrystalline cellulose* (45%)
 - *α -lactose-monohydrate* (45%)
 - *carbomer* (4.25%)
 - *hydroxyethylcellulose* (0.75%)
10. Optimal process parameter recommendations in laboratory scale are:
 - 1000 ml glass pelletizing bowl
 - Initial temperature: 25°C
 - 100.0 g net weight of powders before liquid addition
 - 3 min premixing time
 - 5 min net pelletizing time
 - 1 min mixing after binder addition
 - 24 h drying of samples before examinations

- 500 rpm impeller speed
- 2000 rpm chopper speed
- 10ml/min binder flow rate (purified water)
- 50 ml total amount of binder liquid

7. Conclusion

During first experimental part the high-shear pelletization, the impeller speed and binder flow rate were observed as critical manufacturing parameters influencing the average particle size. Considering the formation of agglomerates, while the binder flow rate had a positive quadratic effect on the average particle size, the action of impeller was more complex depending on its rotation speed. The examined NIR diffuse reflectance spectra of pellet samples offer a fast instrumental method for in-process control and they can be due to the changed scattering which depended on the particle size of pellets. This experiment served as a base to adjust high-shear process variables according to therapeutical aims of my second experiment, focused on the gastrointestinal candidiasis therapy which is in accordance with the scientific literature.

The second part of my experimental work focused on the optimization of the *nystatin* based pharmaceutical therapy in GIC. Considering the parameters to be optimized, enhanced drug release and long contact time are the most important in terms of successful medication. The application of carbomer, a commonly used mucoadhesive excipient and hydroxyethylcellulose, a high stability and compatibility mucoadhesive agent in the optimized proportion in combination with optimized pellet size may be the key to a successful GIC therapy. According to the response surfaces obtained from the experimental design, the average pellet size of 550 μm , 85% carbopol: 15% hydroxyethylcellulose ratio (4.25% CPL and 0.75% HEC content) are approaching the optimal therapeutic effect, which result in approximately 50–55% bioadhesion retention, $\tau = 5\text{--}10$ min drug release, β value of 0.32–0.37 and swelling index above 5%.

These estimations were confirmed in our test production where further investigations of the dosage form were carried out in order to prepare the applicant sample as a possibility for a more successful therapy in GIC.

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